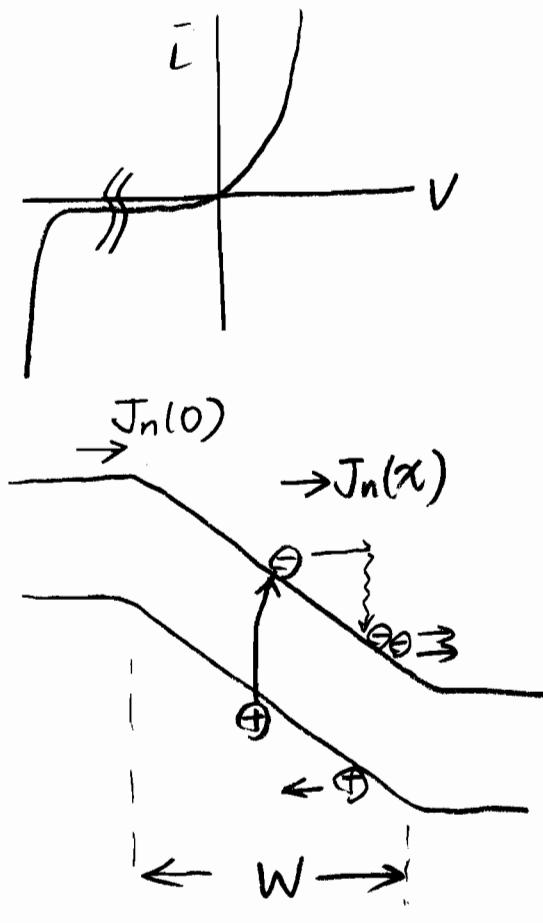


# Avalanche Photodetector (APD)

Biased near reverse breakdown



Avalanche:

Energetic electron (hole)  
release its kinetic energy  
by generating an additional  
electron-hole  
⇒ Impact ionization

Impact ionization coef.

{ for electron :  $\alpha_n$  ( $\text{cm}^{-1}$ )

{ for hole :  $\beta_p$  ( $\text{cm}^{-1}$ )

; # of e-h pair generated  
by one incident electron  
(hole)

Ideal case:

Electron impact ionization only

$$\frac{dJ_n(x)}{dx} = \alpha_n J_n(x)$$

$$J_n(x) = J_n(0) \cdot e^{\alpha_n x}$$

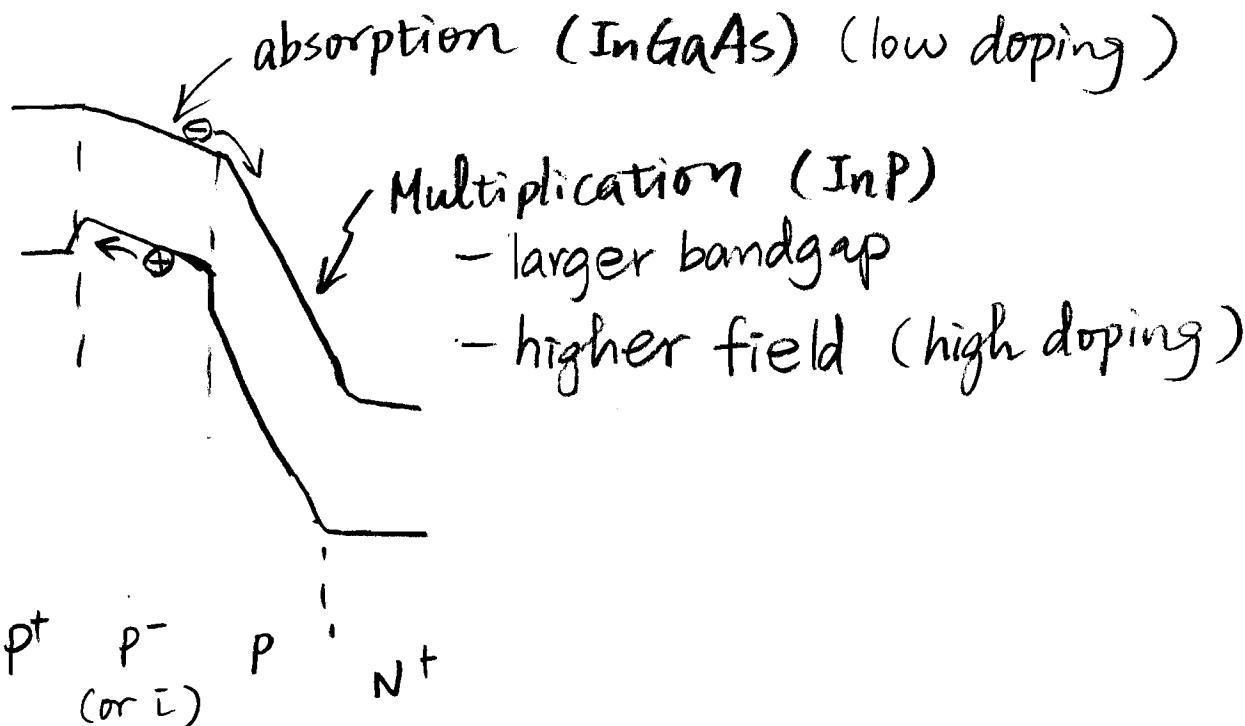
At  $x=W$ , electron current only

$$J = J_n(x=W) = J_n(0) e^{\alpha_n W} = M_n \cdot J_n(0)$$

$$M_n = e^{\alpha_n W} = \text{Multiplication factor}$$

Usually separate absorption and multiplication  
(SAM) structure is used for APD

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- \* Only electrons enter the multiplication region
- \* Photo-generated holes are collected directly.
- \* In the multiplication region, additional holes as well as electrons are generated.
  - Holes could gain kinetic energy and cause impact ionization too

## Analysis of multiplication region

$$\frac{d}{dx} J_n(x) = \alpha_n J_n(x) + \beta_p J_p(x) \quad \dots \textcircled{1}$$

↑                      ↑                      ↑  
 electron current    electron impact    hole impact  
 ionization            ionization          ionization

$$-\frac{d}{dx} J_p(x) = \alpha_n J_n(x) + \beta_p J_p(x) \quad \dots \textcircled{2}$$

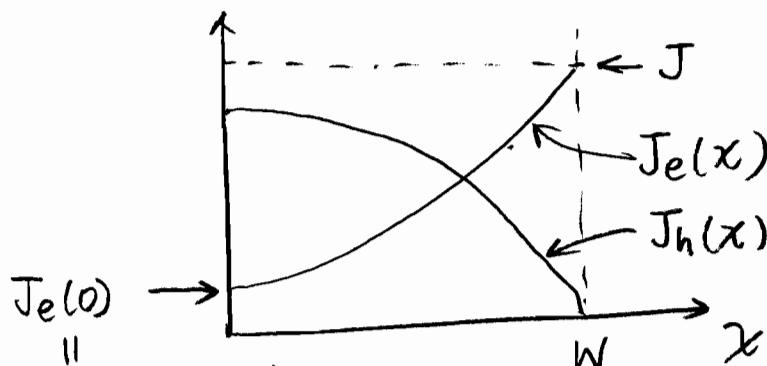
$$\textcircled{1} - \textcircled{2} : \frac{d}{dx} (J_n(x) + J_p(x)) = 0$$

$$J_n(x) + J_p(x) = J = \text{const} \quad (\text{KCL})$$

$$J_p(x) = J - J_n(x)$$

$$\frac{d}{dx} J_n(x) - \alpha_n J_n(x) - \beta_p (J - J_n(x)) = 0$$

$$\frac{d}{dx} J_n(x) - [\alpha_n - \beta_p] J_n(x) = \beta_p J$$



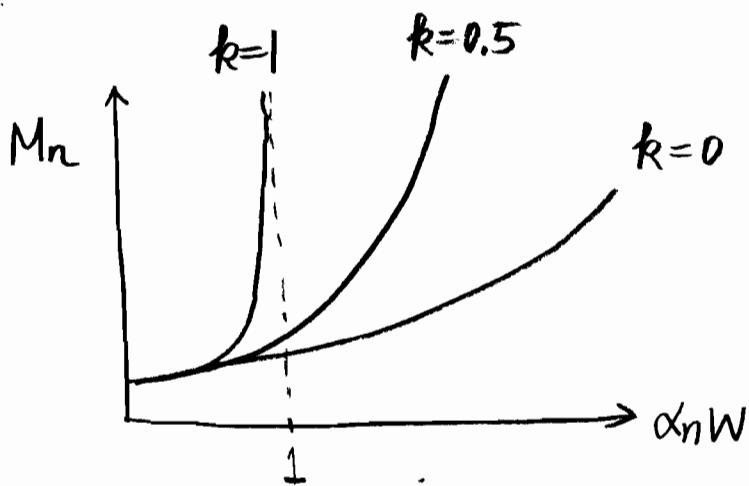
$J_e(0)$   
 photocurrent  
 density  
 from absorption region

Multiplication Factor (Eq. 14.4.27b in Chuang)

$$\begin{aligned}
 M_n &= \frac{J}{J_n(0)} = \frac{1}{1 - \int_0^W dx' \cdot \alpha_n \cdot e^{-(\alpha_n - \beta_p)x'}} \\
 &= \frac{1}{1 - \frac{\alpha_n}{\alpha_n - \beta_p} (1 - e^{-(\alpha_n - \beta_p)W})} \\
 &= \frac{\alpha_n - \beta_p}{\alpha_n e^{-(\alpha_n - \beta_p)W} - \beta_p}
 \end{aligned}$$

Let  $k = \frac{\beta_p}{\alpha_n}$

$$M_n = \frac{1-k}{e^{-(1-k)\alpha_n W} - k}$$



$k=1$ ,  $M_n \rightarrow \infty$  at  $\alpha_n W = 1 \Rightarrow$  unstable

$k \ll 1$ , Stable gain with lower noise

## Response Time

$$\tau = \tau_t + \tau_m$$

↑                   ↑  
 transit      multiplication  
 time              time  
 in absorption

$$\tau_m = \frac{M_n k W}{V_e} + \frac{W}{J_h} \approx \frac{M_n k W}{V_e} \quad \text{when } M_n \gg 1$$

$$\tau \approx \tau_m$$

Gain-bandwidth product

$$G \times BW = M_n \cdot \left( \frac{1}{2\pi} \frac{1}{\tau_m} \right) = M_n \frac{1}{2\pi} \frac{V_e}{M_n k W} = \frac{1}{2\pi} \frac{V_e}{k W}$$

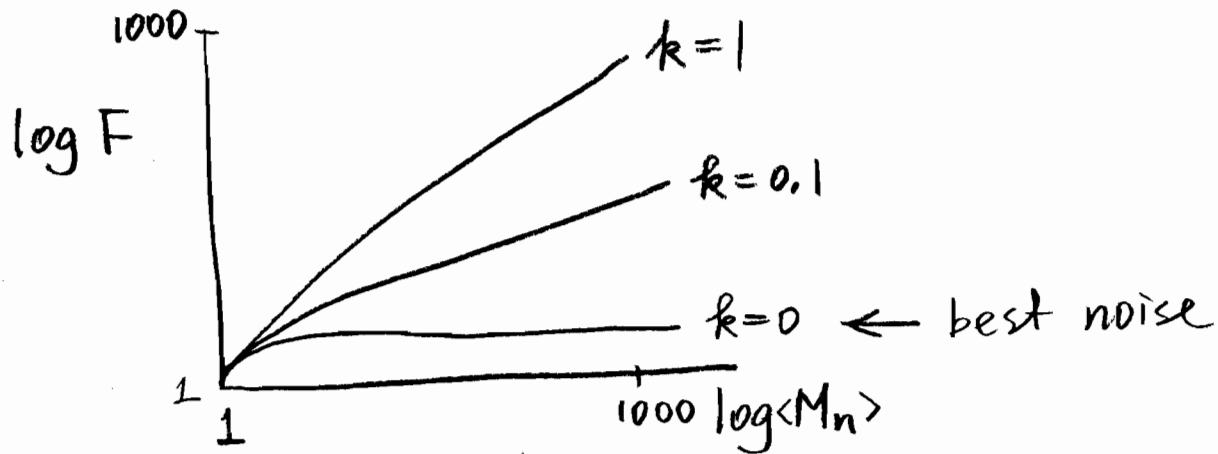
= const

# APD Excess Noise

Fluctuation in gain M

Excess noise factor

$$F = \frac{\langle M^2 \rangle}{\langle M \rangle^2} = k \langle M_n \rangle + (1-k) \left( 2 - \frac{1}{\langle M_n \rangle} \right)$$



Small  $k \rightarrow$  smaller F @ high gain

$F_{min}$  at high gain = 2 when  $k=0$

$\Rightarrow$  Minimum noise figure = 3 dB

$$\text{APD signal } \bar{i}_p = 2 \frac{g}{\hbar w} P \langle M \rangle = \bar{i}_{p_0} \cdot \langle M \rangle$$

↑  
average optical power

Shot noise

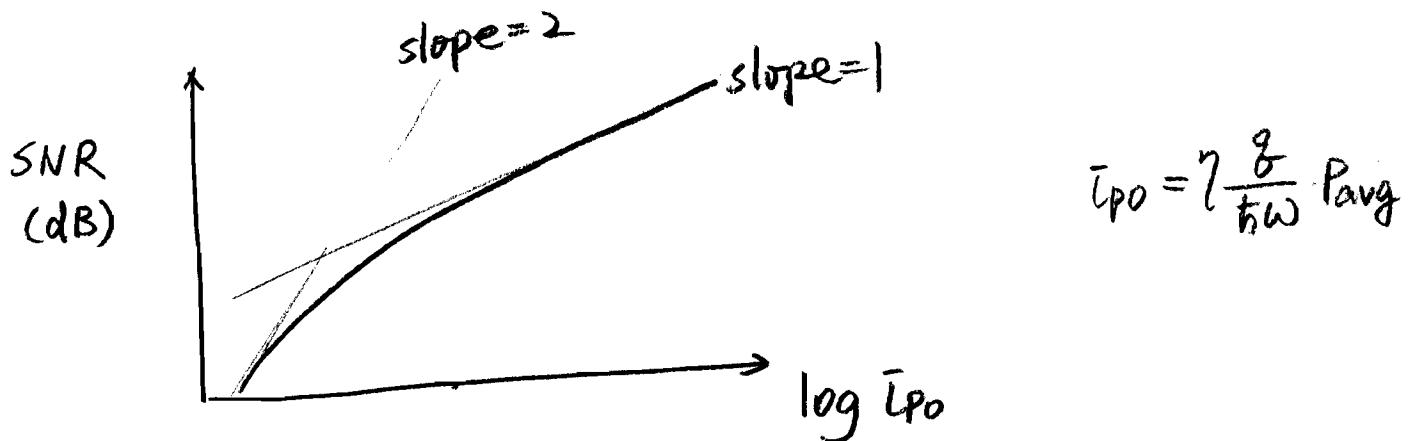
$$\begin{aligned}\langle \bar{i}_s^2 \rangle &= 2g \bar{i}_{p_0} \langle M^2 \rangle \cdot \Delta f \\ &= 2g \bar{i}_{p_0} \langle M \rangle^2 \cdot F \cdot \Delta f\end{aligned}$$

shot noise is multiplied by gain  $\langle M \rangle^2$   
and further multiplied by excess noise factor

Thermal noise

$$\langle \bar{i}_T^2 \rangle = \frac{4k_T T}{R} \Delta f$$

$$SNR = \frac{\bar{i}_p^2}{\langle \bar{i}_s^2 \rangle + \langle \bar{i}_T^2 \rangle} = \frac{\bar{i}_{p_0}^2 \langle M \rangle^2}{2g \bar{i}_{p_0} \langle M \rangle^2 \cdot F \cdot \Delta f + \frac{4k_T T}{R} \Delta f}$$



$$\text{For small } \bar{i}_{p_0}, SNR \rightarrow \frac{\bar{i}_{p_0}^2 \langle M \rangle^2}{\left(\frac{4k_T T}{R}\right) \Delta f} \propto \bar{i}_{p_0}^2$$

$$\text{large } \bar{i}_{p_0}, SNR \rightarrow \frac{\bar{i}_{p_0}}{2g \cdot F \Delta f} \propto \bar{i}_{p_0}$$

SNR for p-i-n is the same expression with

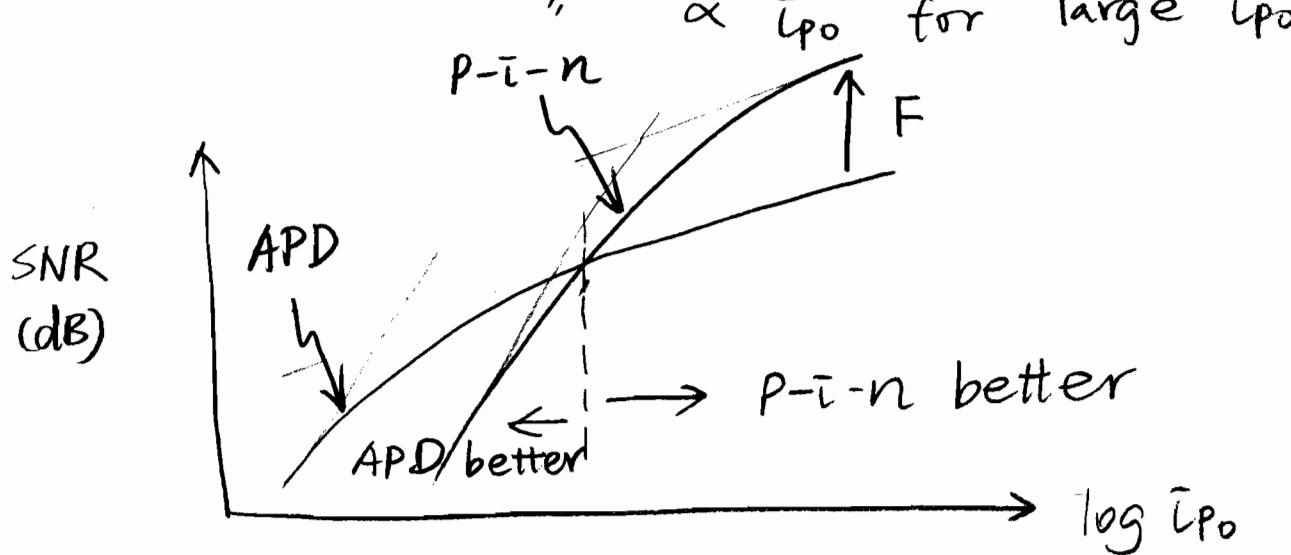
$$\langle M \rangle = 1$$

$$F = 1$$

$$SNR_{p-i-n} = \frac{\bar{I}_{p_0}^2}{2g\bar{I}_{p_0}\Delta f + \frac{4kT}{R}\Delta f}$$

Similarly.  $SNR_{p-i-n} \propto \bar{I}_{p_0}^2$  for small  $\bar{I}_{p_0}$

"  $\propto \bar{I}_{p_0}$  for large  $\bar{I}_{p_0}$



At high photocurrent ( $\bar{I}_{p_0}$ ).  $\frac{SNR_{p-i-n}}{SNR_{APD}} = F$

P-i-n better

At low photocurrent ( $\bar{I}_{p_0}$ ), thermal noise dominant in p-i-n.

APD has higher SNR  $\Rightarrow$  APD better

Cross Point

$$SNR_{APD} = SNR_{P-I-n}$$

$$\frac{\cancel{\bar{I}_{p_0}^2 \langle M \rangle^2}}{(2g \cancel{\bar{I}_{p_0} \langle M \rangle^2 F} + \frac{4k_T T}{R}) \Delta f} = \frac{\cancel{\bar{I}_{p_0}^2}}{(2g \cancel{\bar{I}_{p_0}} + \frac{4k_T T}{R}) \Delta f}$$

$$\Rightarrow 2g \bar{I}_{p_0} F + \frac{4k_T T}{R} \cdot \frac{1}{\langle M \rangle^2} = 2g \bar{I}_{p_0} + \frac{4k_T T}{R}$$

$$\Rightarrow \bar{I}_{p_0} = \frac{\frac{4k_T T}{R} (1 - \frac{1}{\langle M \rangle^2})}{2g(F-1)}$$

\*

Example

$$k=0.2, \alpha_n W = 1.9$$

$$M = M_n = \frac{1-k}{e^{-(1-k)\alpha_n W} - k} = 42.8$$

$$F = k \cdot M + (1-k) \left( 2 - \frac{1}{M} \right) = 10$$

$$\bar{I}_{p_0} = 2 \underbrace{\frac{k_T T}{g}}_{0.026V} \cdot \frac{1}{R} \cdot \frac{1}{F-1} = 1.1 \times 10^{-4} \approx 110 \mu A$$

↑  
50Ω \*