

- 10.7 (a) The increases of $\ln J_{th}$ with inverse cavity length $1/L$ are because the decrease of the cavity length L will increase the threshold gain, $g_{th} = \alpha_i + \frac{1}{2L} \ln \frac{1}{R_1 R_2}$.

The slope is determined by L_{opt} as shown in (10.3.39).

$$L_{opt} = \frac{1}{2} \frac{1}{n_w \Gamma_w g_0} \ln \left(\frac{1}{R_1 R_2} \right)$$

- (b) With a given number of quantum wells n_w , the optimal cavity length is L_{opt} which depends on n_w , Γ_w , g_0 , R_1 , and R_2 .

- (c) Assume: $J_0 = 200 \text{ A/cm}^2$ $g_0 = 3000 \text{ cm}^{-1}$ $\Gamma_w = 0.02$
 $\alpha = 20 \text{ cm}^{-1}$ $R_1 = R_2 = 0.3$ $\eta = 0.8$ $W = 2 \text{ } \mu\text{m}$

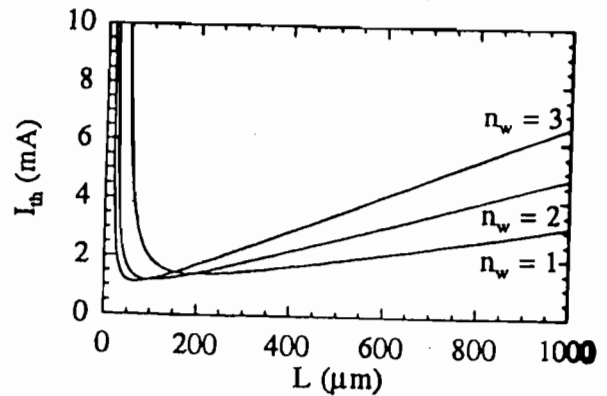
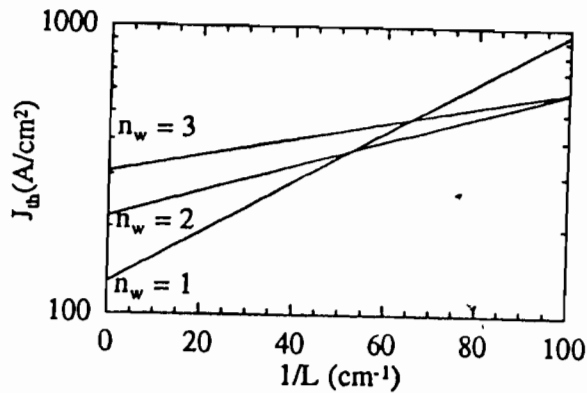
$$L_{opt} = \frac{1}{2} \frac{1}{n_w \Gamma_w g_0} \ln \left(\frac{1}{R_1 R_2} \right) = \frac{200.7}{n_w} \text{ } \mu\text{m}$$

$$\begin{aligned} \ln J_{th} &= \ln \left(\frac{n_w J_0}{\eta} \right) + \frac{\alpha}{n_w \Gamma_w g_0} + \frac{L_{opt}}{L} - 1 \\ &= \ln J_0 + \left(\ln n_w - \ln \eta + \frac{\alpha}{n_w \Gamma_w g_0} - 1 \right) + \frac{L_{opt}}{L} \end{aligned}$$

$$\ln \frac{J_{th}}{J_0} = \left(\ln n_w + \frac{1}{3n_w} - 0.777 \right) + \frac{L_{opt}}{L}$$

$$\frac{J_{th}}{W L J_0} = \frac{n_w}{\eta} \exp \left[\frac{1}{n_w \Gamma_w g_0} \left(\alpha + \frac{1}{2L} \ln \frac{1}{R_1 R_2} \right) - 1 \right]$$

The plots corresponding to Figs. 10.25(a) and (b) are shown below.



10.8 Assume single subband pair, $n = C_1$, $m = hh_1$

$$g(\hbar\omega) = \begin{cases} g_m [f_c - f_v] & \hbar\omega > E_{e1} - E_{h1} + E_g \\ 0 & \hbar\omega < E_{e1} - E_{h1} + E_g \end{cases}$$

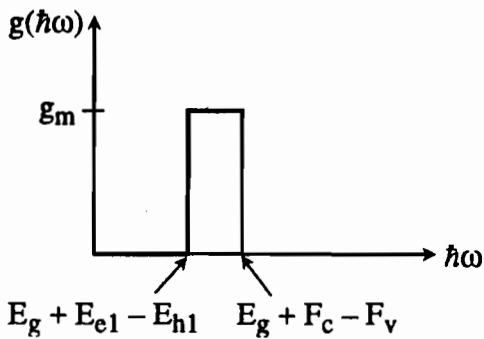
$$g_m = C_0 |\hat{e} \cdot \mathbf{M}|^2 \rho_r^{2D} = \frac{\pi e^2}{n_r c \epsilon_0 m_0^2 \omega} \left(\frac{3}{2} M_b^2 \right) \frac{m_r}{\pi \hbar^2 L_z} = 6254 \text{ cm}^{-1} \text{ (Assume: } \hbar\omega \approx E_g \text{)}$$

TE polarization

$$f_c = \frac{1}{1 + \exp \left[\frac{E_{e1} + (\hbar\omega - E_{e1} + E_{h1} - E_g) \frac{m_r}{m_c^*} - F_c}{k_B T} \right]}$$

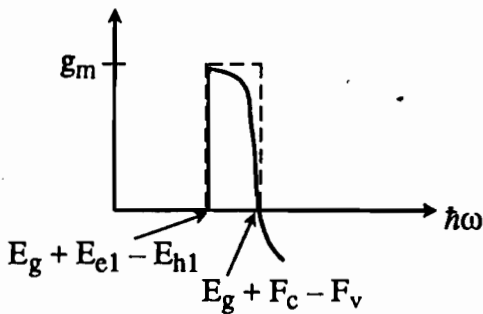
$$f_v = \frac{1}{1 + \exp \left[\frac{E_{h1} + (\hbar\omega - E_{e1} + E_{h1} - E_g) \frac{m_r}{m_h^*} - F_v}{k_B T} \right]}$$

If assume $T = 0 \text{ K} \Rightarrow f_c = \begin{cases} 1 & \hbar\omega < F_c - F_v + E_g \\ 0 & \hbar\omega > F_c - F_v + E_g \end{cases} \quad f_v = \begin{cases} 0 & \hbar\omega < F_c - F_v + E_g \\ 1 & \hbar\omega > F_c - F_v + E_g \end{cases}$



[Note: F_c and F_v are determined from injection carrier concentrations $n = p$.]

If $T \neq 0$



10.9 (a) single subband (C1 and HH1), $T = 300 \text{ K}$, $L_z = 100 \text{ \AA}$

$$n_c = \frac{m_e^* k_B T}{\pi \hbar^2 L_z} = 7.18 \times 10^{17} \text{ cm}^{-3} \quad (m_e^* = 0.0665 m_0)$$

$$n_v = \frac{m_h^* k_B T}{\pi \hbar^2 L_z} = 3.67 \times 10^{18} \text{ cm}^{-3} \quad (m_h^* = m_{hh}^* = 0.034 m_0)$$

$$\begin{aligned} \text{(b) } f_c = f_v &\Rightarrow 1 - \exp\left(-\frac{n_{tr}}{n_c}\right) = \exp\left(-\frac{n_{tr}}{n_v}\right) \\ &\Rightarrow n_{tr} = 10.18 \times 10^{17} \text{ cm}^{-3} = 1.02 \times 10^{18} \text{ cm}^{-3} \end{aligned}$$

10.10 The number of quantum wells can be chosen by drawing a horizontal line that corresponds to the desired threshold gain on Fig. 10.24(b), and then by selecting the number of quantum wells that will give a minimized current density of the crossing point of the gain curve and the horizontal line.

For example, as shown in the left plot, the optimum number is 1 for $g_{th} = g_1$, and is 2 for $g_{th} = g_2$.

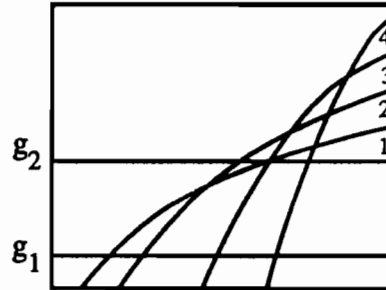


Fig. 10.24(b)