



13th Workshop on Crystalline Solar Cell Materials and Processes
August 2003, Vail, Colorado



Failure of Silicon: Crack Formation and Propagation

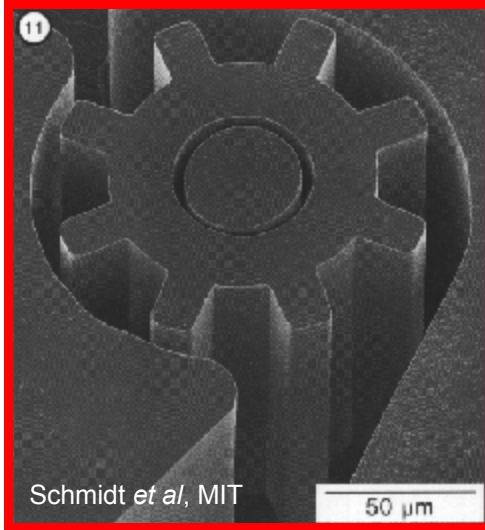
Robert O. Ritchie

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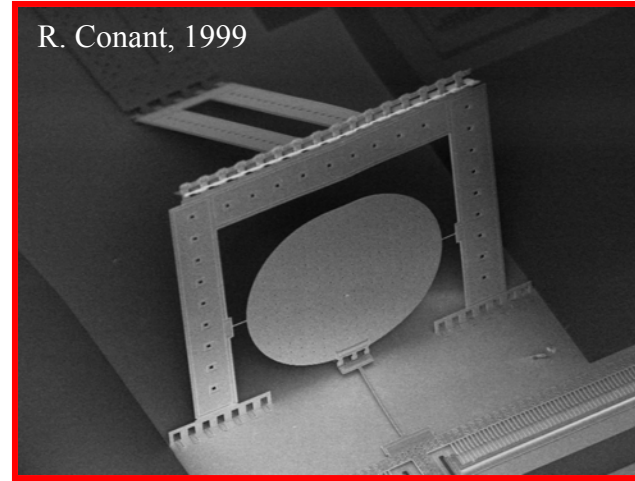
with thanks to

C. L. Muhlstein (*Penn State*) and **E. A. Stach** (*NCEM, LBNL*)

Work supported by the U.S. Department of Energy (Basic Energy Sciences), NEDO and Exponent, Inc.



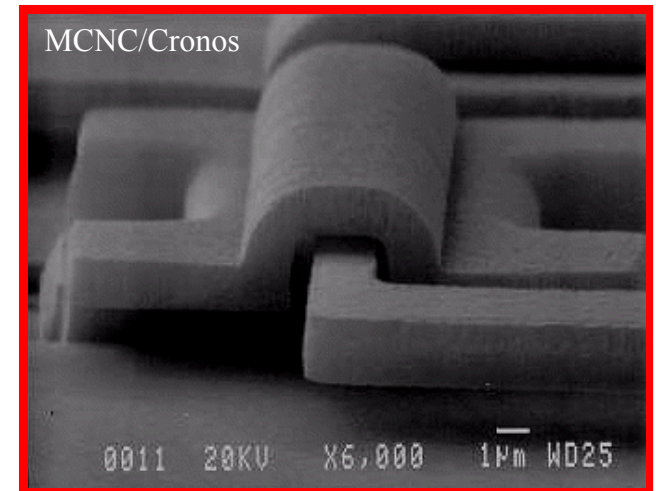
microturbine,



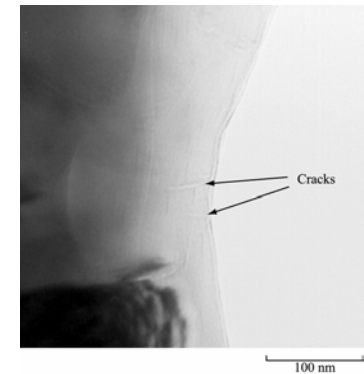
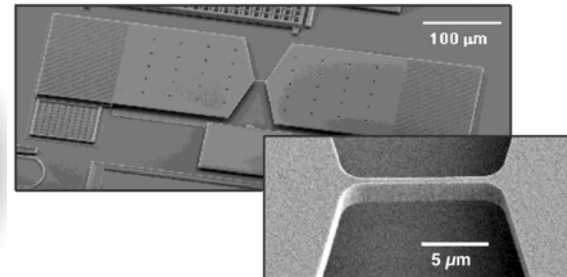
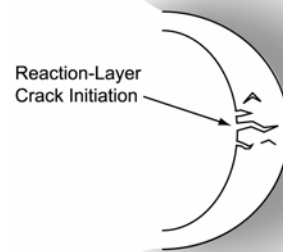
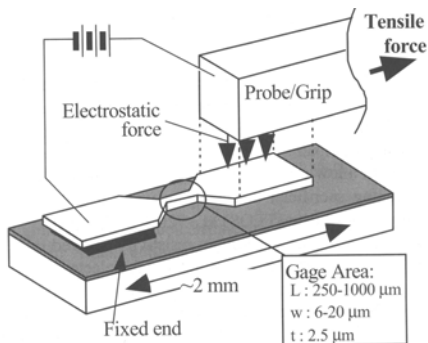
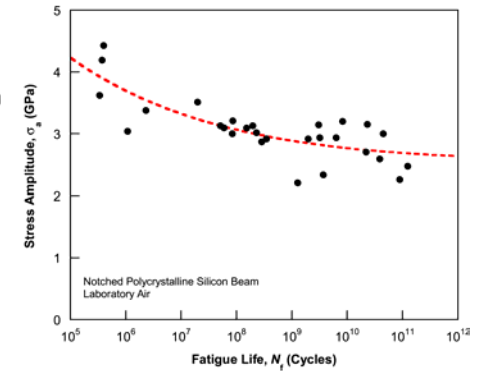
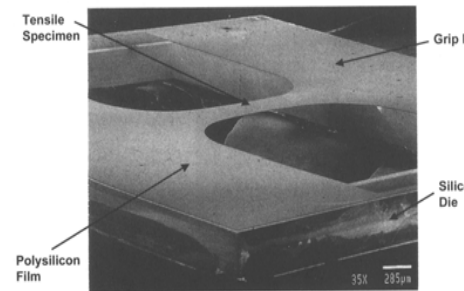
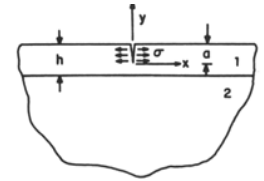
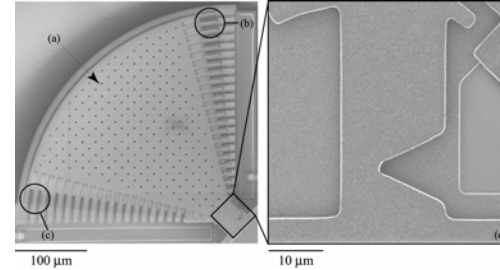
micron-scale
moveable mirrors



microhinge



- Mechanical properties of silicon
- Brittle fracture of silicon
- Strength vs. fracture toughness
- Delayed failure of thin-film silicon
- Role of the native oxide layer
- Suppression/prediction of fracture





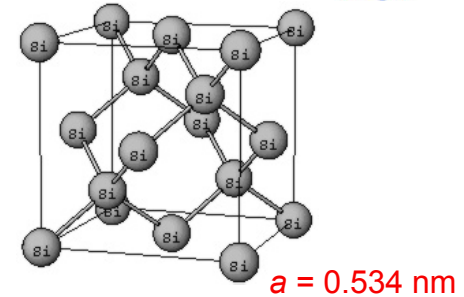
Ductile vs. Brittle Properties of Silicon



- crystal structure

- diamond cubic structure (face-centered cubic)

- brittle-to-ductile transition (DBTT at $\sim 500^\circ\text{C}$)



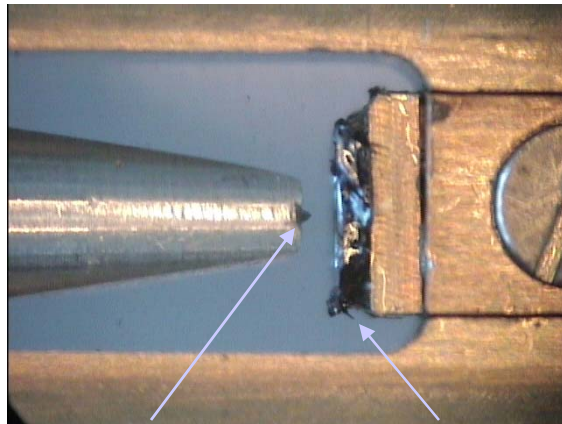
- below the DBTT (or at high strain rates), Si is completely brittle

- dislocations not mobile, Si fractures by cleavage on $\{111\}$ planes
 - fracture strengths ~ 1 to 20 GPa in single-crystal silicon
 - fracture strengths ~ 3 to 5 GPa in polycrystalline silicon

- above the DBTT, silicon becomes gradually ductile

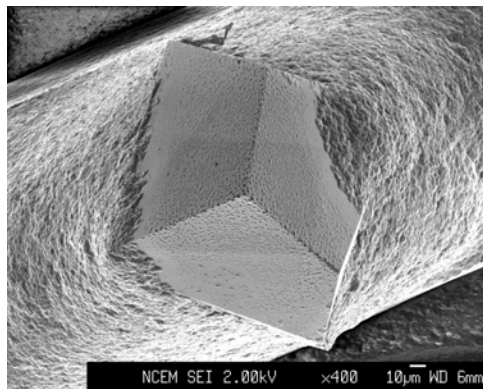
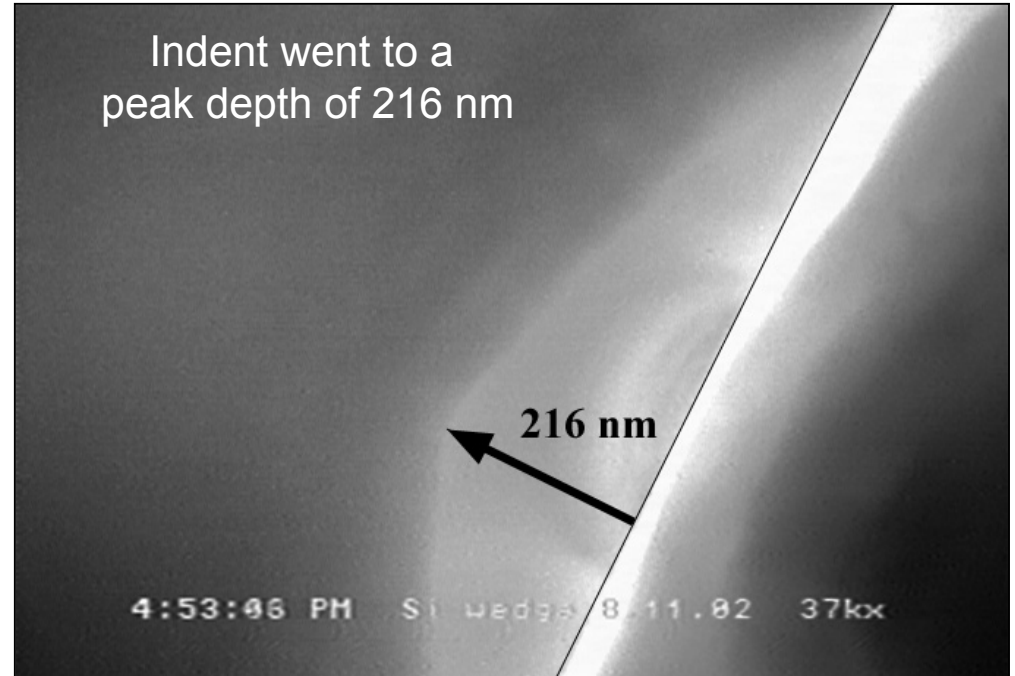
- glide motion of $(a/2)\langle 110 \rangle$ dislocations on $\{111\}$ planes
 - dissociation into $(a/6)\langle 112 \rangle$ Shockley partials with 4-6 nm stacking faults
 - heterogeneous dislocation nucleation in “dislocation-free” crystals
 - e.g., at surfaces or due to deformation-induced amorphous Si
 - solid-solution hardening by impurity solutes, e.g., oxygen, nitrogen

Mobile Dislocations in Silicon at 25°C

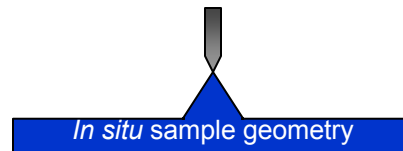


diamond

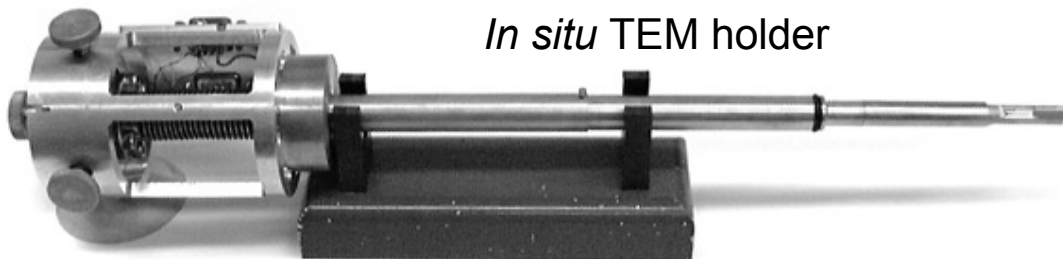
sample



indenter



In situ TEM holder



- no phase transformations
- large plastic extrusions of the diamond cubic phase
- dislocation nucleation easier than phase transformation



Modes of Failure in Silicon



- Brittle (catastrophic) fracture
 - catastrophic transgranular cleavage fracture on $\{111\}$ planes
 - evidence for $\{110\}$ cleavage for “low energy/velocity” fractures
- Sustained-load cracking (delayed fracture)
 - no evidence for delayed fracture from subcritical crack growth, e.g., due to stress-corrosion cracking, in *bulk* silicon below the DBTT ($<500^{\circ}\text{C}$)
 - evidence for moisture-induced cracking in *thin film* silicon
- Cyclic fatigue failure (delayed fracture)
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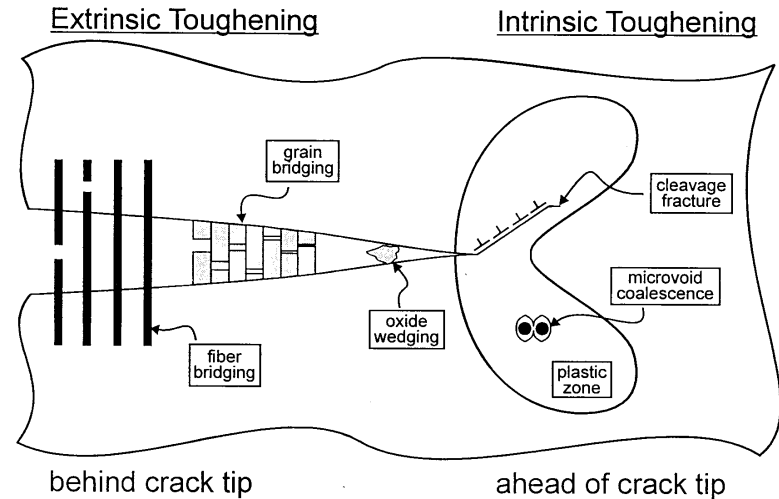
What affects resistance to brittle fracture? in silicon?

- Intrinsic factors

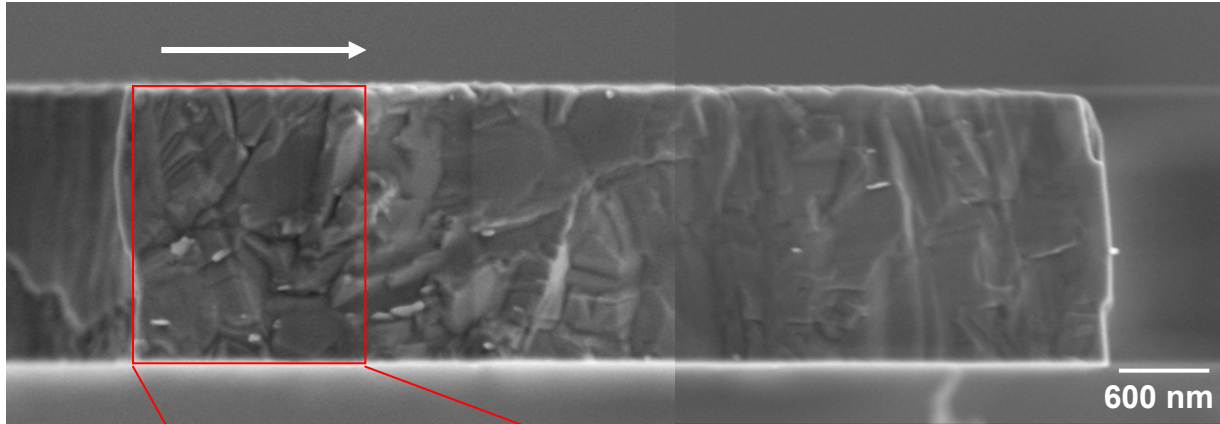
- bond rupture
- plasticity, i.e., mobile dislocations
- defect (crack) population

- Toughening mechanisms

- intrinsic mechanisms (ahead of crack tip)
 - microstructure, e.g., second phases
- extrinsic (crack-tip shielding) mechanisms (behind crack tip)
 - crack bridging (intergranular cracking)
 - microcrack toughening (from dilation and reduced stiffness)
 - residual stresses (compressive for toughening)



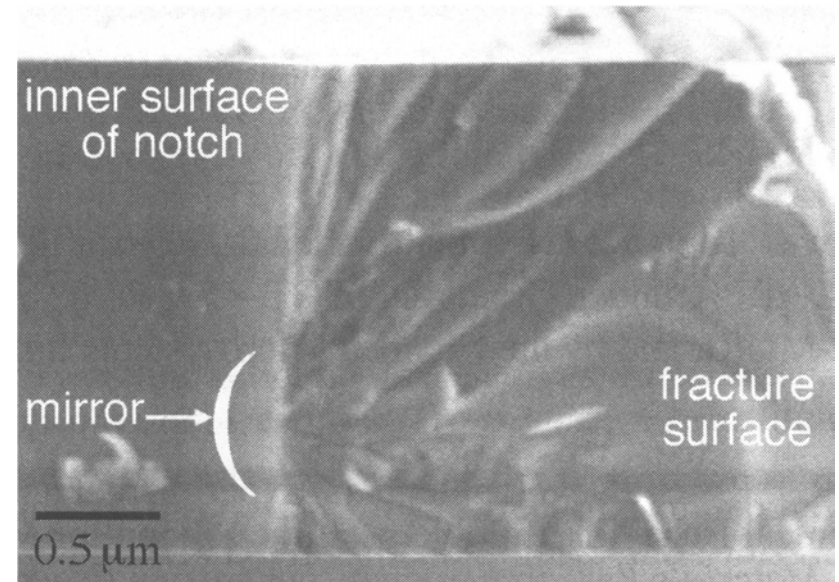
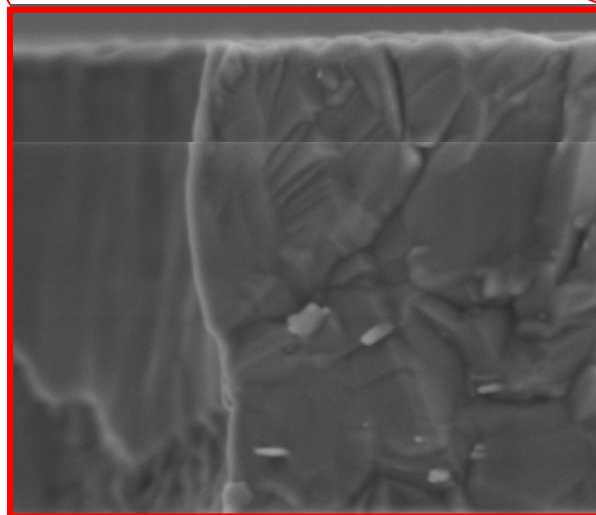
Brittle Fracture of Silicon



transgranular
cleavage
fracture

{111} cleavage

{110}
cleavage



Muhlstein, Brown, Ritchie, *Sensors & Actuators*, 2001

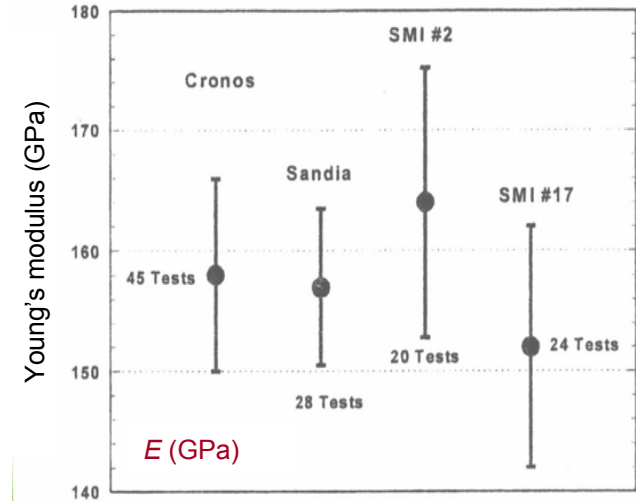
Ballarini *et al.*, ASTM STP 1413, 2001



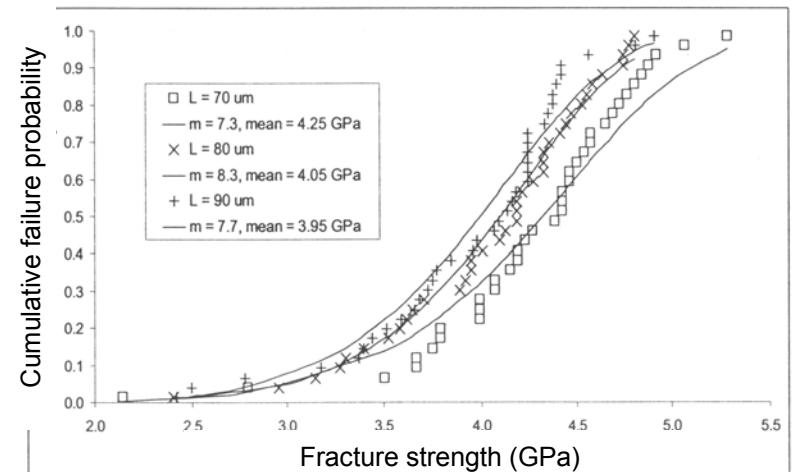
Brittle Fracture of Silicon



- elastic modulus
 - $E \sim 160$ GPa
- high fracture strengths
 - 1 to 20 GPa in single-crystal silicon
 - 3 to 5 GPa in polycrystalline silicon
 - dependent on *defect size*, loading mode, specimen size, orientation, test method
 - probability of fracture dependent on “weakest-link” (Weibull) statistics
- low fracture toughness
 - $K_c \sim 1$ MPa \sqrt{m} in polysilicon thin films
 - $K_c \sim 0.7$ - 1.3 MPa \sqrt{m} in single-crystal films
 - dependent on specimen type, orientation and investigator
 - *independent of microstructure*



Sharpe et al., ASTM STP 1413, 2001



Johnson et al., ASTM STP 1413, 2001



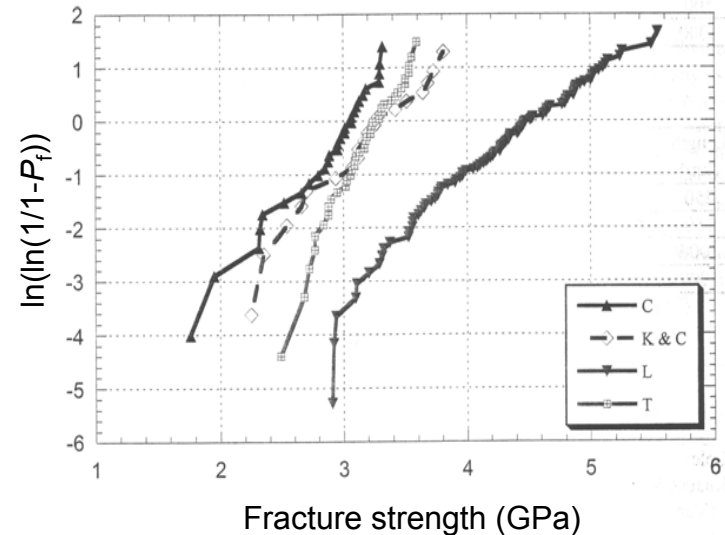
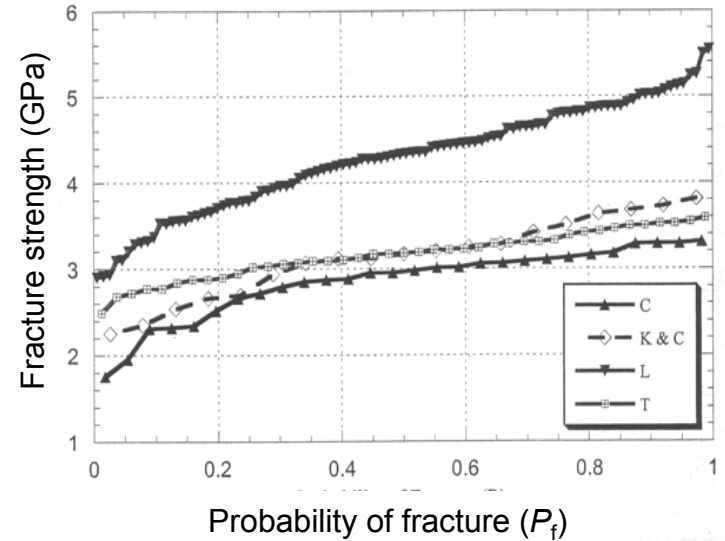
Probability of Brittle Fracture in Silicon



- brittle fracture of silicon governed solely by the rupture of Si-Si bonds at the crack tip
 - K_c is independent of microstructure
- except variations due to orientation (in single-crystal Si) and experimental error, *fracture strength depends on the defect population*
- The probability of failure, P_F , can thus best be described in terms of “weakest-link” statistics

$$P_F(\sigma) = 1 - \exp \left[- \int_0^V \left[dV \left(\frac{\sigma - \sigma_u}{\sigma_o} \right)^m N \right] \right]$$

- where σ_u is the lower bound fracture strength, σ_o is the “scale parameter”, m is the Weibull modulus, and V is the volume of the sample





Strength vs. Fracture Toughness



- fracture strength/strain subject to extreme variability – not a material property
- more fundamental parameter is the fracture toughness - K_c or G_c
 - where K_c is the critical value of the stress intensity K to cause fracture

$$K_c = Q \sigma_F (\pi a_c)^{1/2}$$

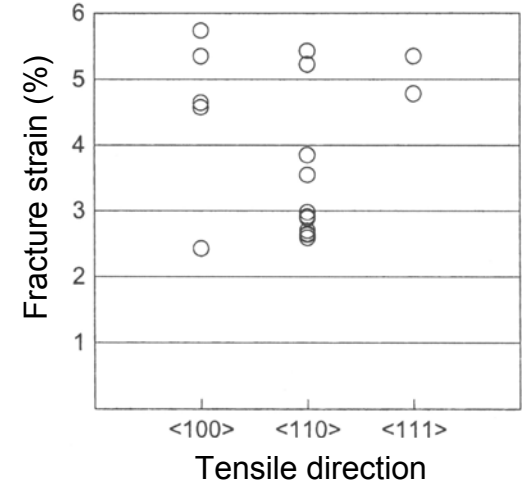
σ_F is the fracture strength
 a_c is the critical crack size
 Q is a geometry factor (\sim unity)

- and G_c is the strain energy release rate

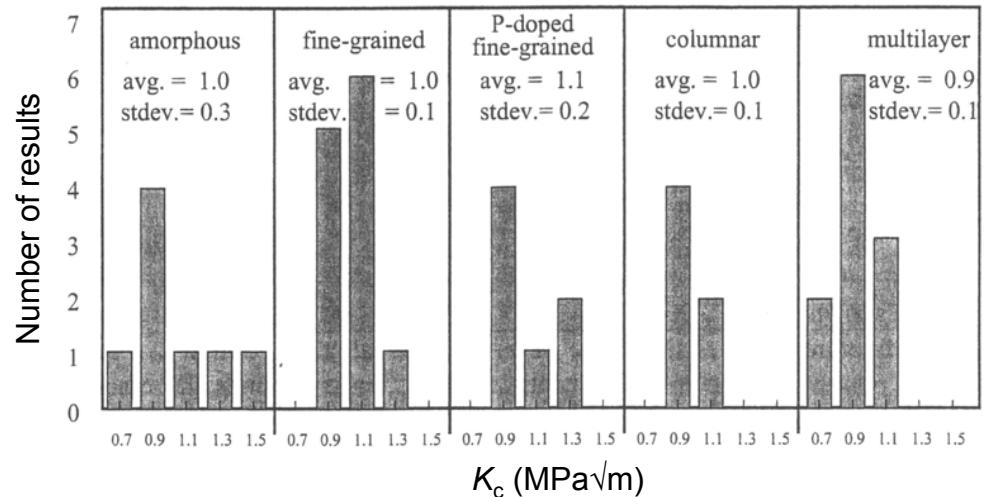
$$G_c = (K_c)^2/E$$

E is Young's modulus

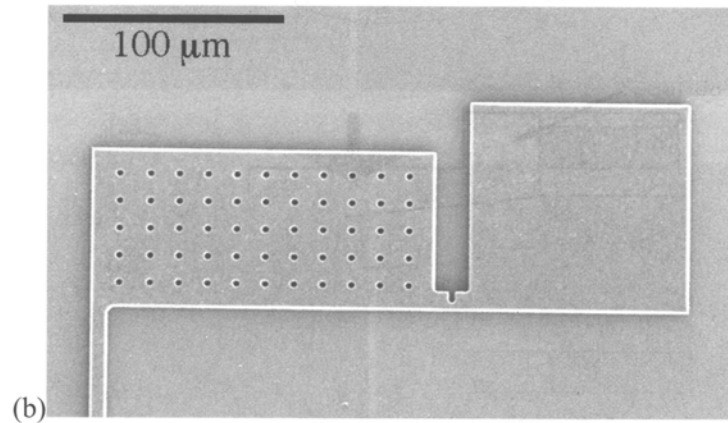
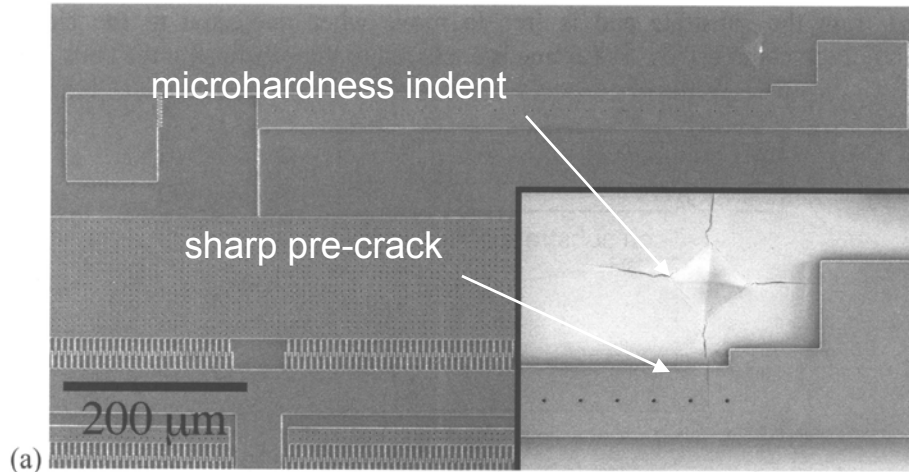
- $K_c = 1 \text{ MPa}\sqrt{\text{m}}$ in Si and is independent of microstructure and dopant



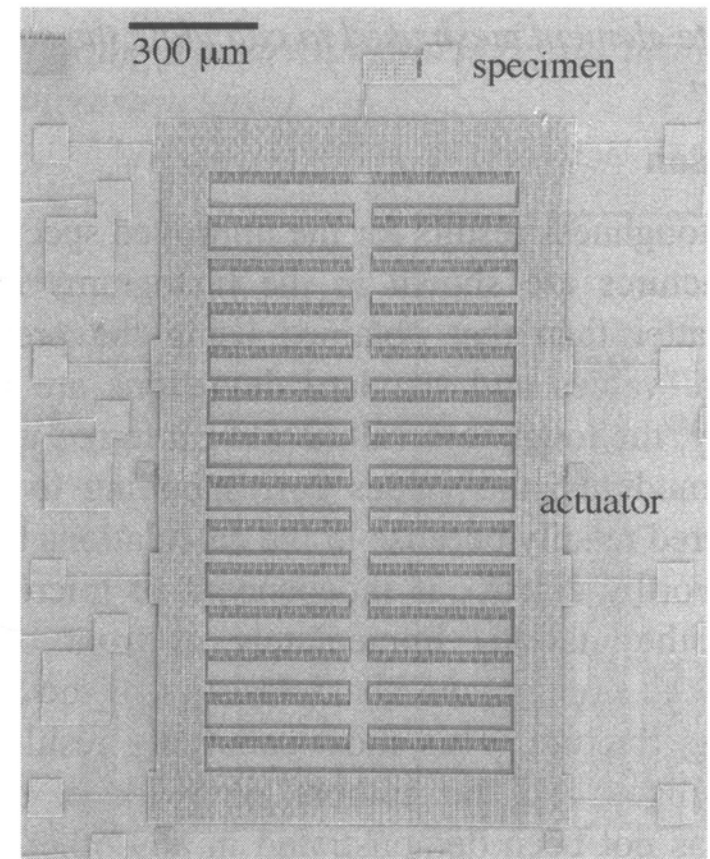
Ballarini *et al.*, ASTM STP 1413, 2001



Measurement of Fracture Toughness



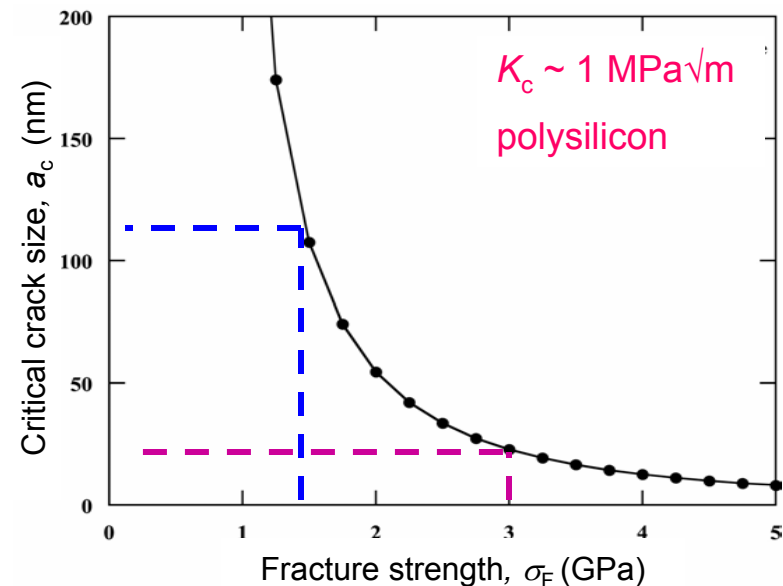
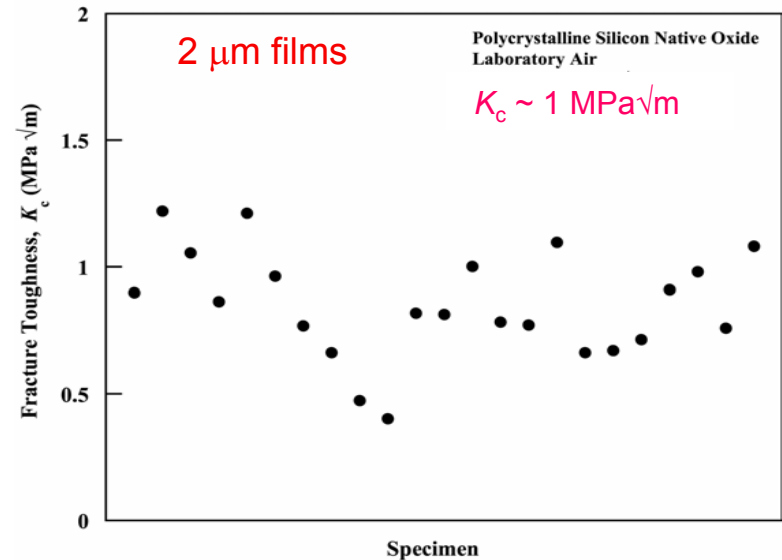
$$K_C = Q \sigma_F (\pi a_C)^{1/2}$$



- measurement of the fracture toughness of thin-film silicon using MEMS

- low fracture toughness K_c in silicon
 - 0.7 to 1.3 $\text{MPa}\sqrt{\text{m}}$ in single-crystal Si
 - 1 $\text{MPa}\sqrt{\text{m}}$ in polysilicon thin films
- compare with K_c values of:
 - $\sim 0.6 \text{ MPa}\sqrt{\text{m}}$ in (soda-lime) glass
 - 2 to 3 $\text{MPa}\sqrt{\text{m}}$ in human teeth (dentin)
 - 3 to 8 $\text{MPa}\sqrt{\text{m}}$ in alumina ceramics
 - 20 to 200 $\text{MPa}\sqrt{\text{m}}$ in steels
- from this microstructure-independent K_c value in Si, can:
 - determine the fracture strength, σ_F , as a function of the largest defect size, a_c

$$K_c = Q \sigma_F (\pi a_c)^{1/2}$$

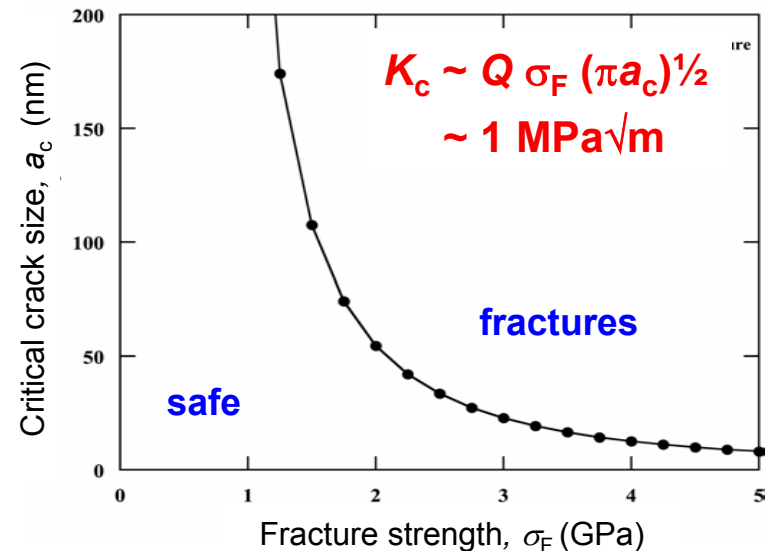
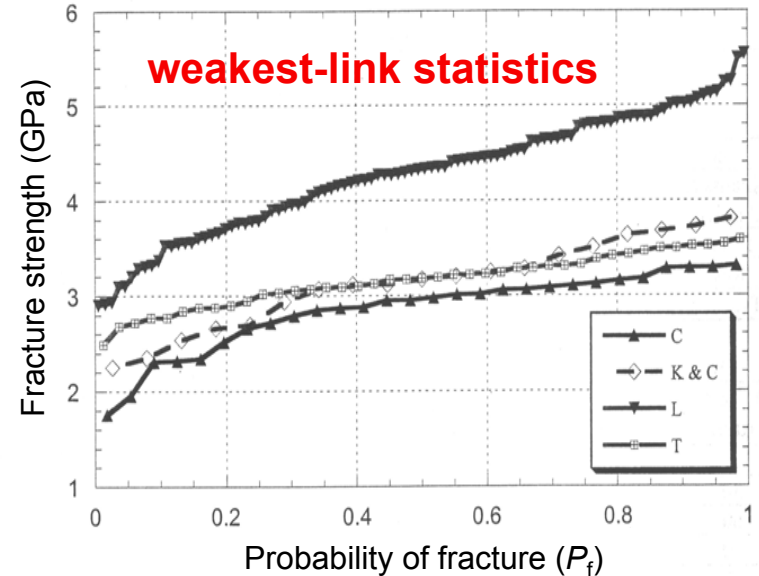




Prediction of Brittle Fracture in Silicon



- **Probability of brittle fracture depends on defect (crack) population**
 - use fracture strength approach with weakest-link statistics to determine probability of fracture
 - characterize defect population at sub-micron resolution (actually tens of nanometers)
 - X-ray tomography (e.g., Xradia, Concord, CA)
 - GHz acoustic microscopy





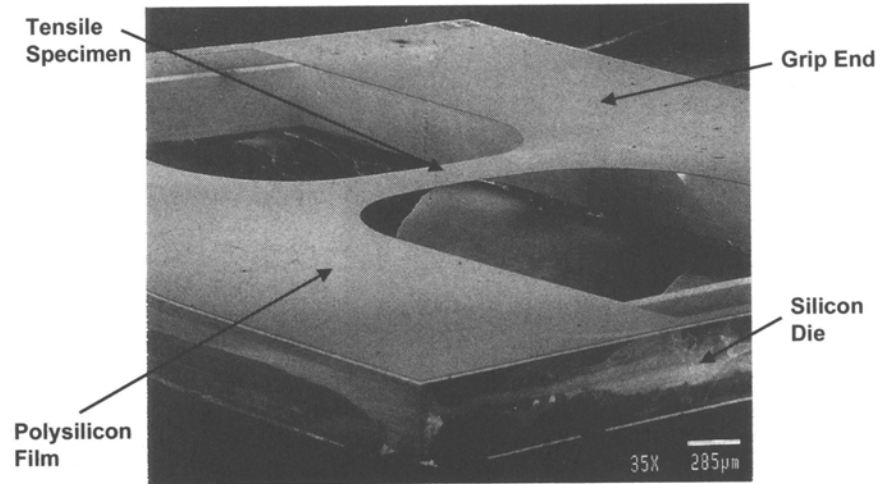
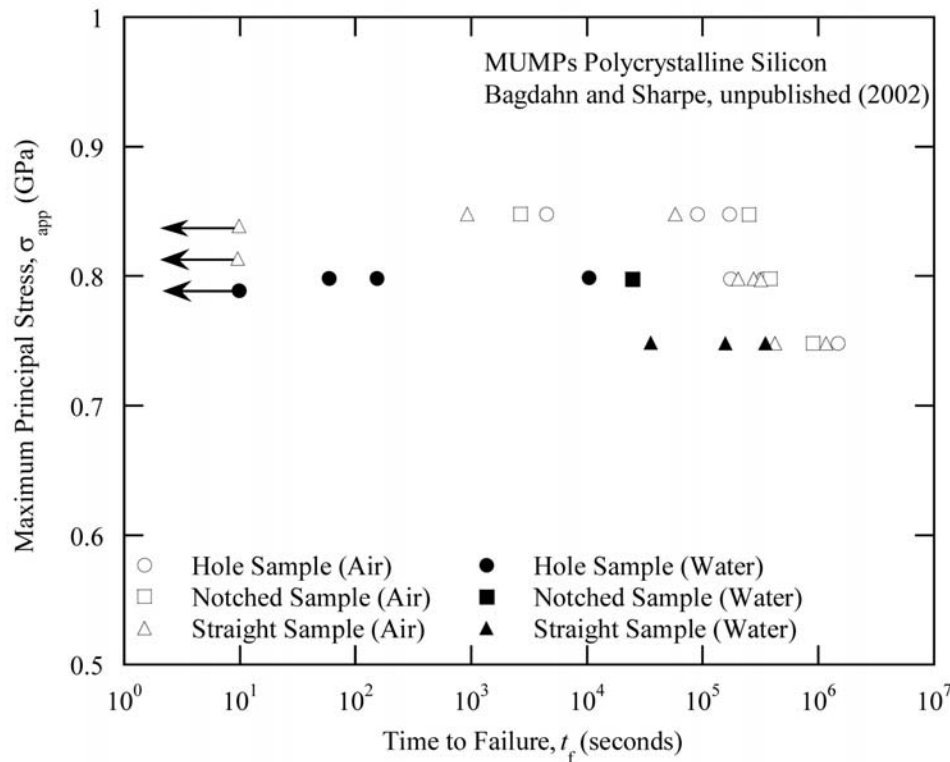
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Environmentally-Assisted Cracking in Polycrystalline Silicon

- micron-scale silicon films display some evidence of time-delayed failure under sustained (non-cyclic) loading



- lives for thin-film silicon are somewhat shorter in water
- no evidence of such time-delayed failure in bulk silicon



Modes of Failure in Silicon



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- composition

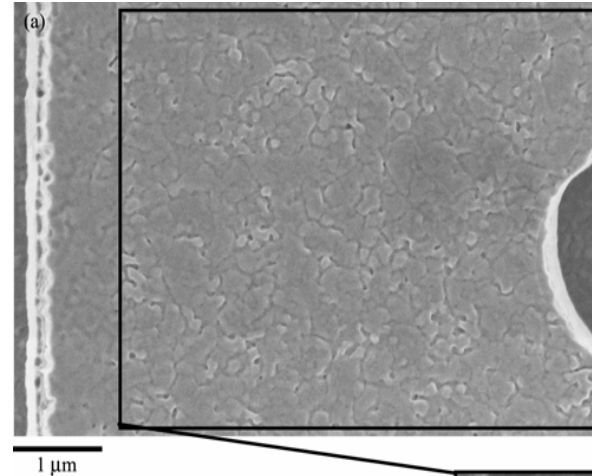
MUMPs process - LPCVD reactor*
 n-type – P doped
 deposited Si and PSG layers
 thermally annealed at $\sim 900^{\circ}\text{C}$

- microstructure

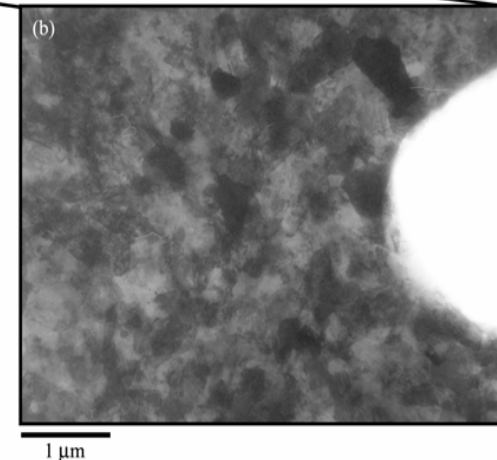
nominal grain size ~ 100 nm
 low residual stresses ~ -9 MPa

- mechanical properties

$E \sim 163$ GPa, $\nu \sim 0.22$
 bending strength, $\sigma_F \sim 3 - 5$ GPa
 fracture toughness $K_{Ic} \sim 1$ MPa $\sqrt{\text{m}}$



low voltage SEM
 uncoated sample



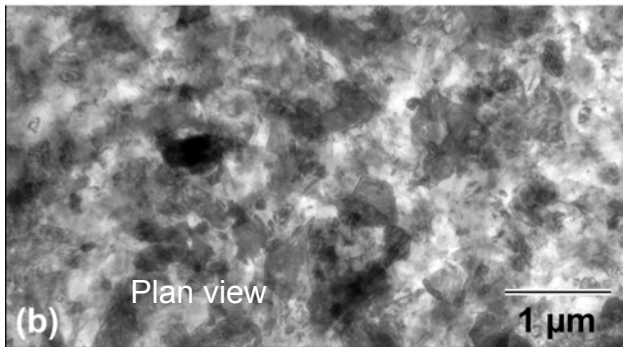
0.8 MeV TEM
 2 μm unthinned
 sample

Contaminants

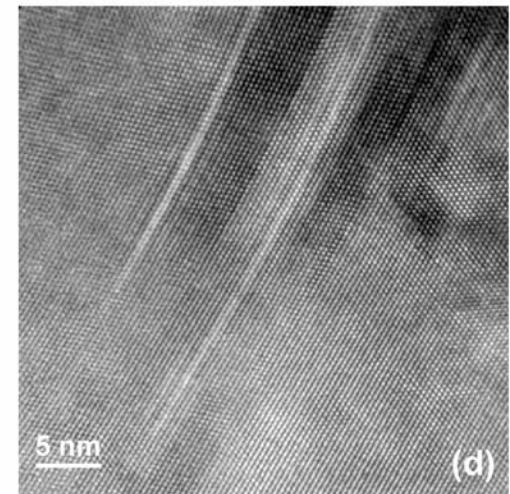
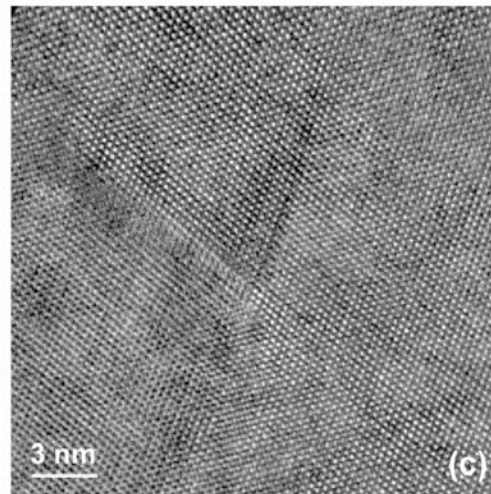
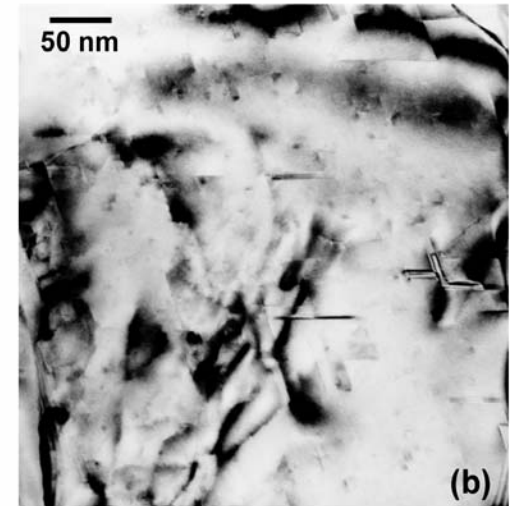
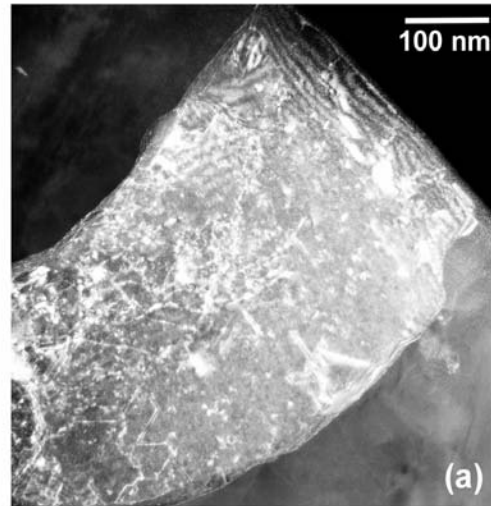
1×10^{19} atoms cm^{-3} P
 2×10^{18} atoms/ cm^{-3} H
 1×10^{18} atoms/ cm^{-3} O
 6×10^{17} atoms/ cm^{-3} C

*MCNC/JDS Uniphase/Cronos/MEMSCAP

Microstructure of Polysilicon Films



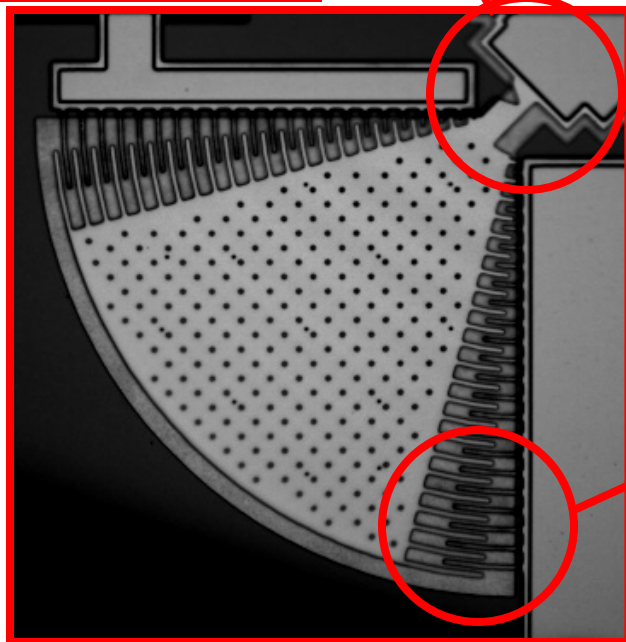
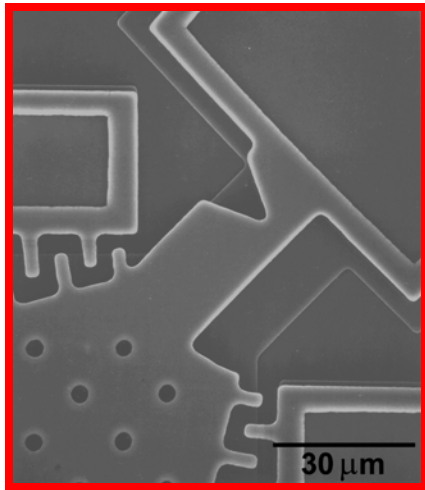
1 MeV HVTEM images



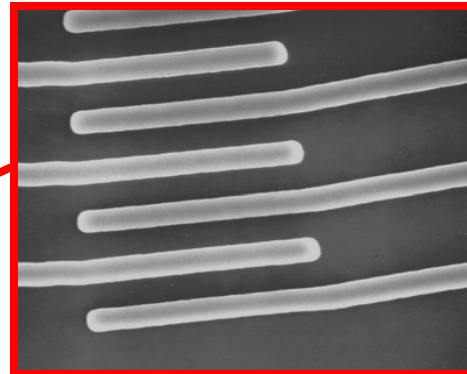
defects in the polysilicon films

- stacking faults
- Lomer-Cottrell locks
- microtwins

Electrostatically-Actuated Resonant Fatigue Testing

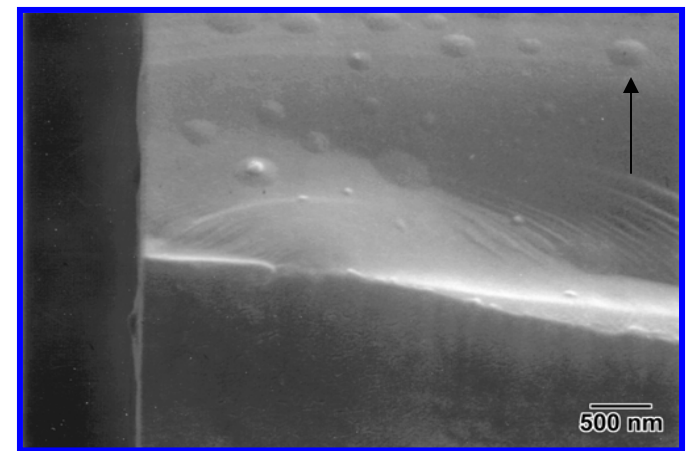
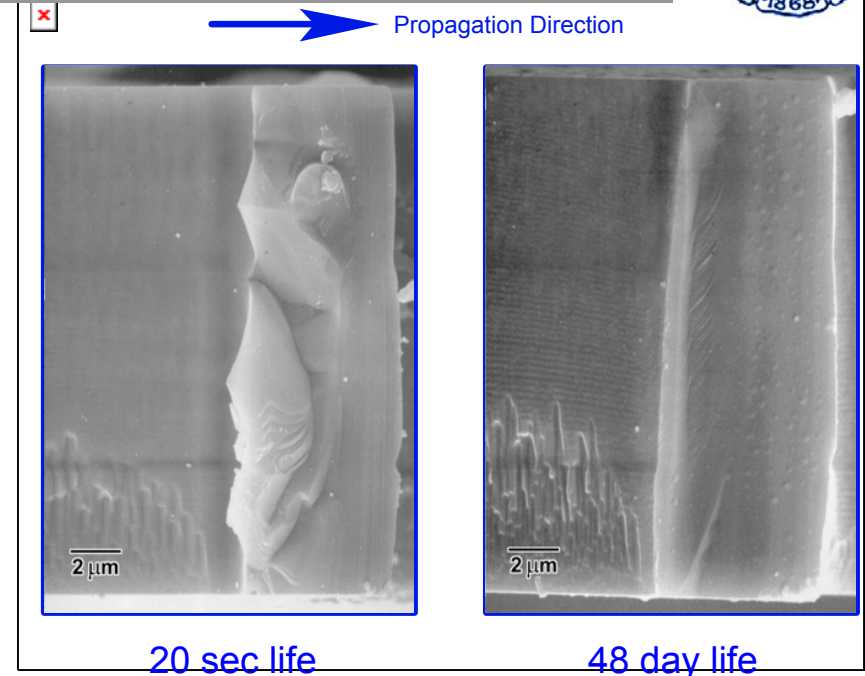
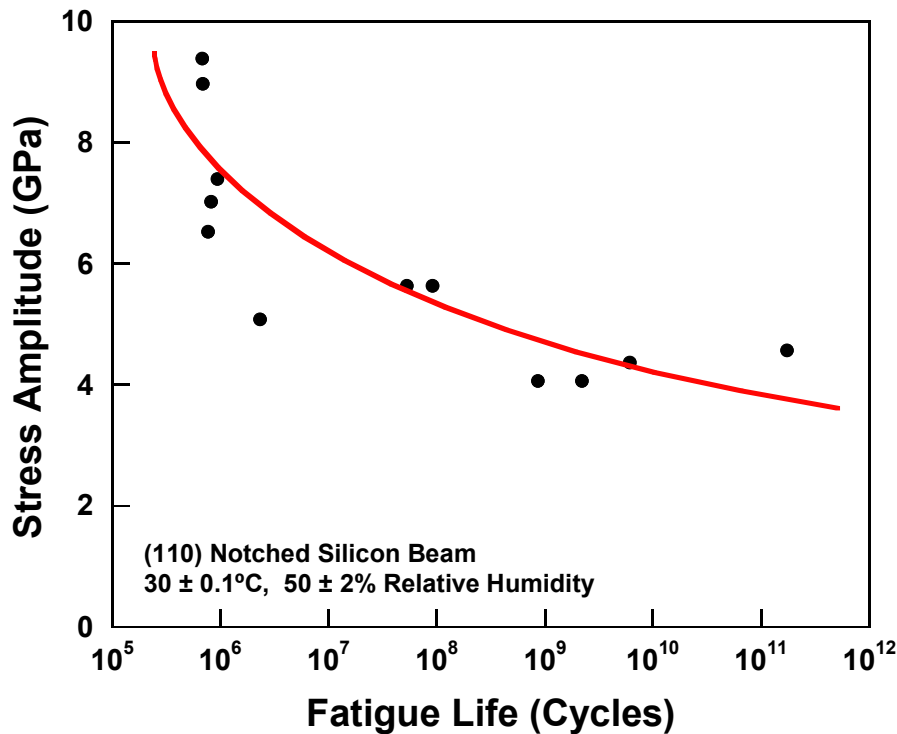


- notched cantilever beam attached to $\sim 300 \mu\text{m}$ square perforated plate (resonant mass)
- “comb drives” on one side are electrostatically forced to resonate at $\sim 40 \text{ kHz}$, with $R = -1$
- other side provides for capacitive sensing of motion, calibrated with machine vision system (Freeman, MIT)
- stress amplitudes determined by finite-element analysis (ANSYS)
- smallest notch root radius ($1 - 1.5 \mu\text{m}$) achieved by photolithographic masking



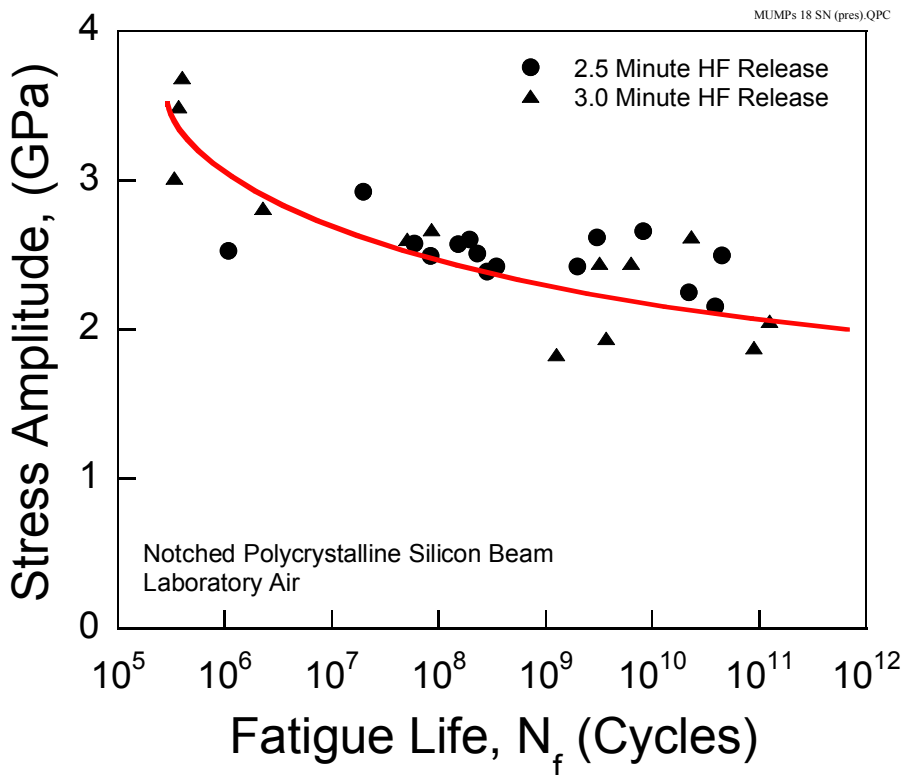
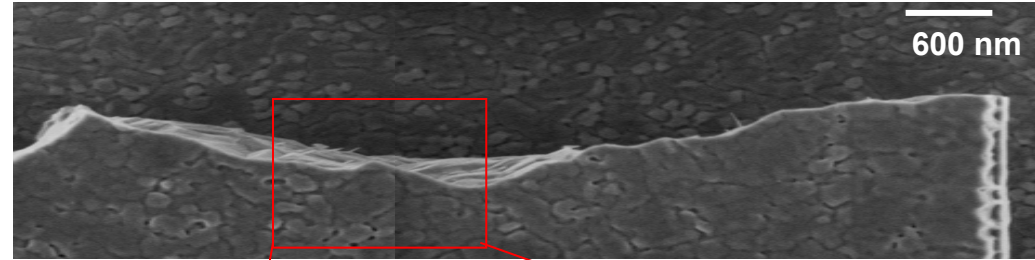
Fatigue of Thin ($20\ \mu\text{m}$) Single Crystal Silicon Films

- Micron-scale p -type (110) single crystal Si films can fail after 10^9 cycles at (maximum principal) stresses (on 110 plane) of one half the (single cycle) fracture strength
- $\{110\}$ crack paths suggest mechanisms other than $\{111\}$ cleavage

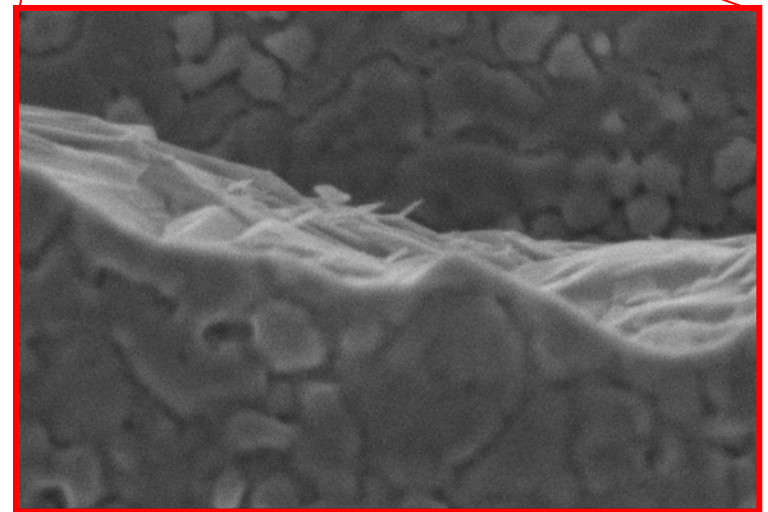


Fatigue of Thin ($2\ \mu\text{m}$) Polycrystalline Silicon Films

- Micron-scale polycrystalline n -type Si is susceptible to fatigue failure
- Films can fail after 10^9 cycles at stresses of one half the (single cycle) fracture strength

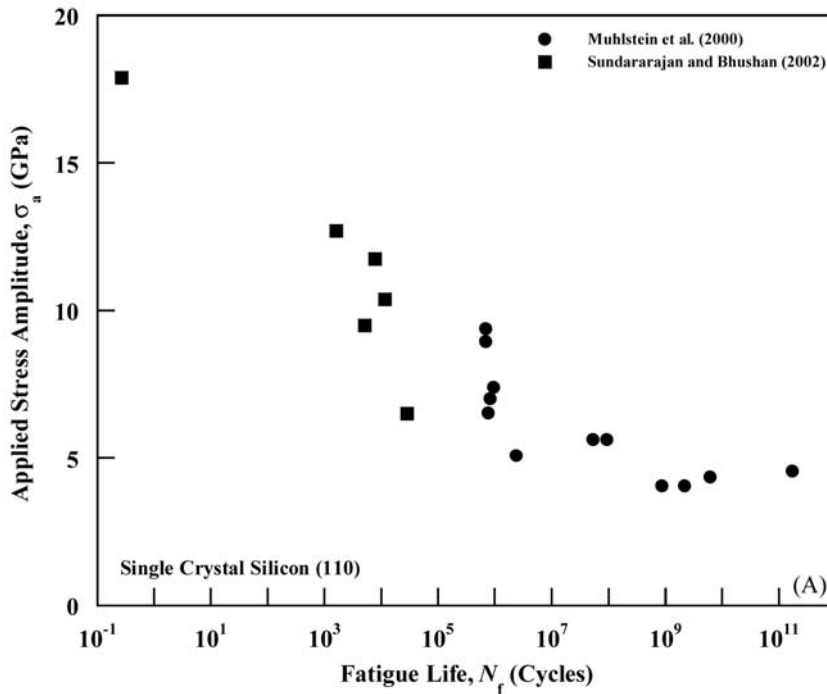


3.8×10^{10} cycles to failure

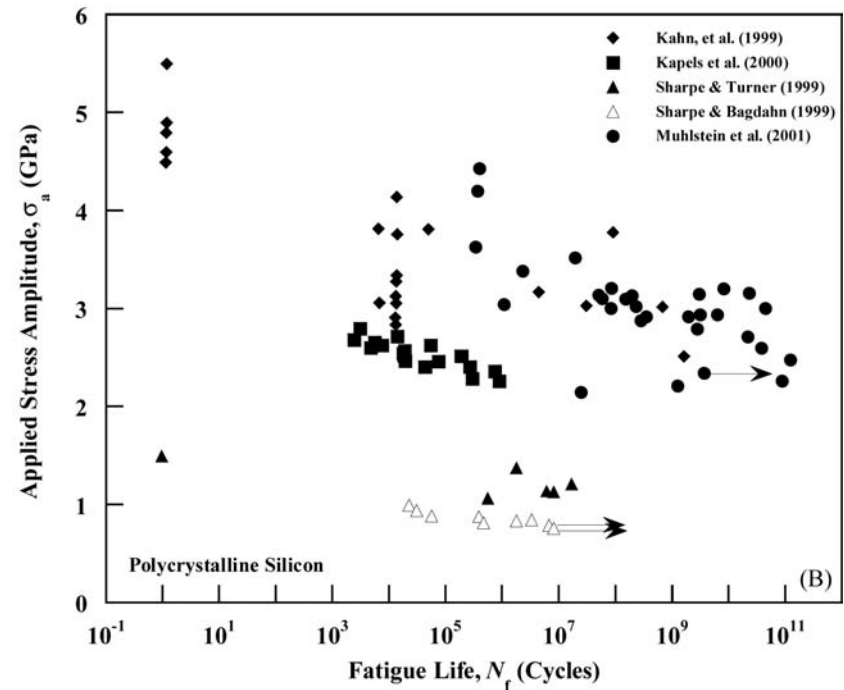


- slivers and debris on fractures consistent with some degree of microcracking

Fatigue of Single Crystal and Polycrystalline Silicon Thin Films



single-crystal (110) silicon

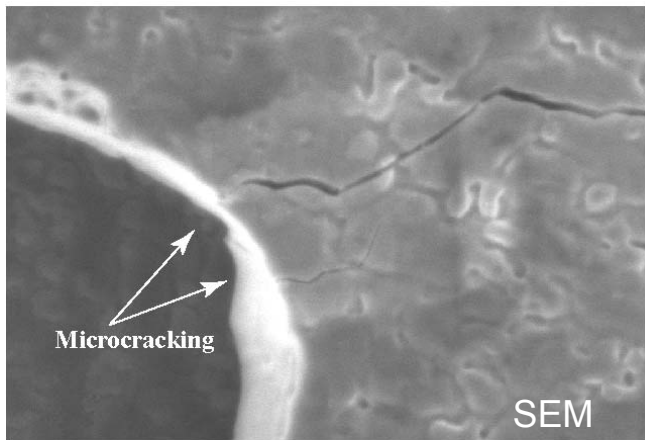


polycrystalline silicon

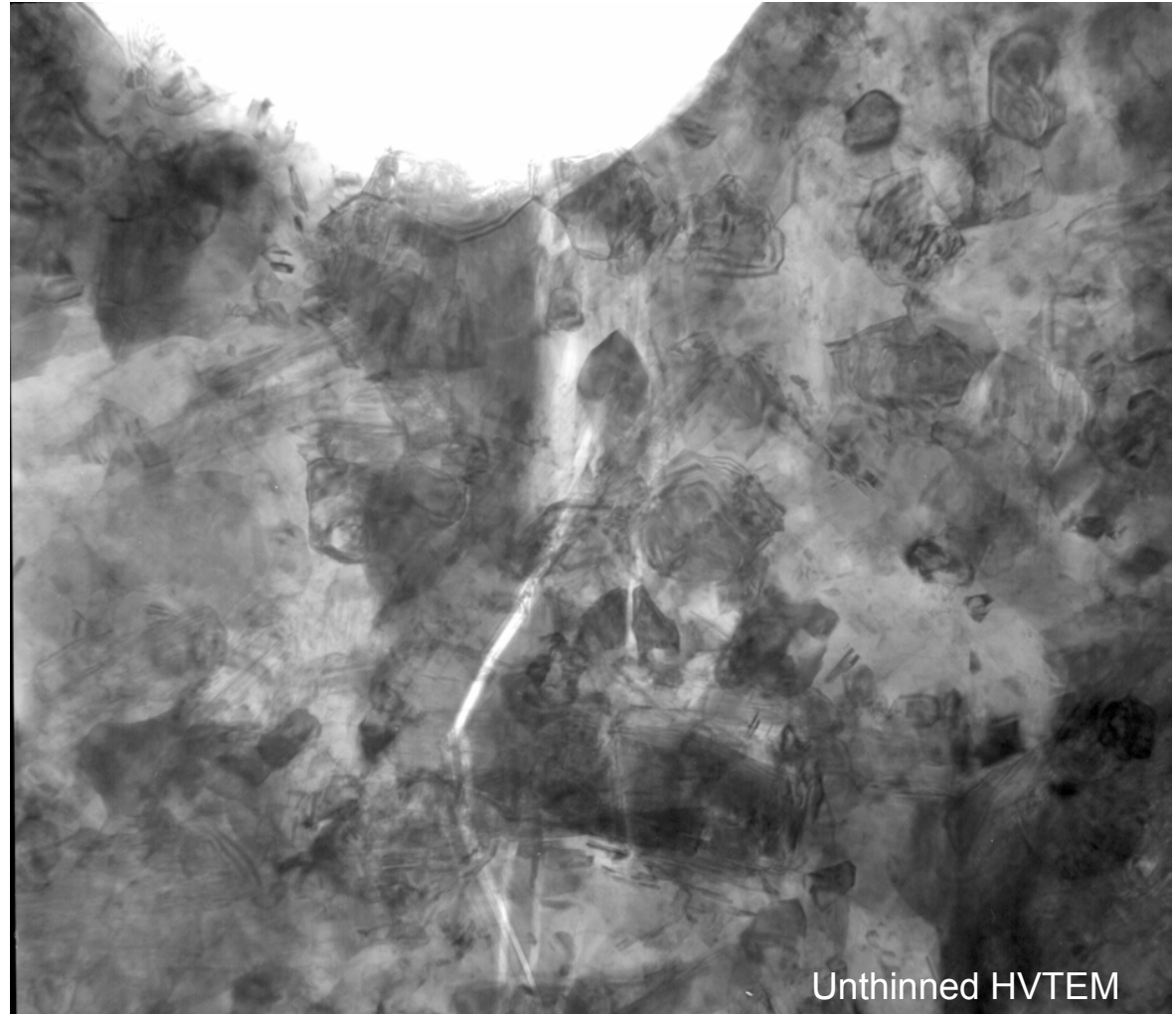
- Micron-scale silicon films display delayed failure under high-cycle fatigue loading
- No such delayed fatigue failure is seen in bulk silicon

Transgranular Cleavage Fracture

- transgranular cleavage cracking from notch under sustained loads
- some evidence of secondary cracking and multiple microcracking



1 μm



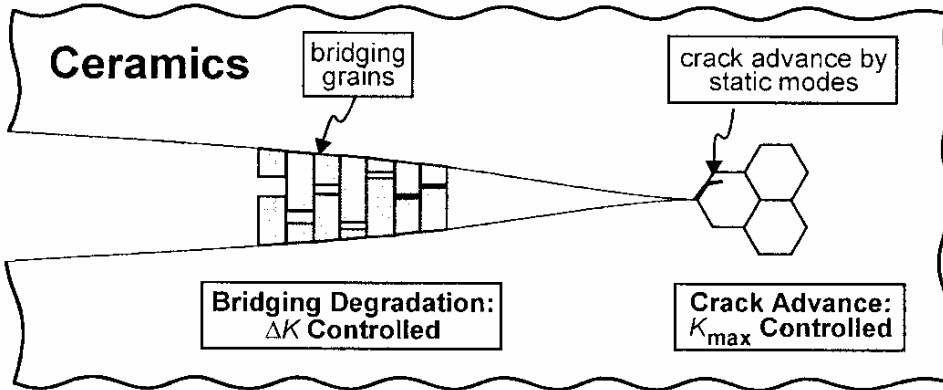
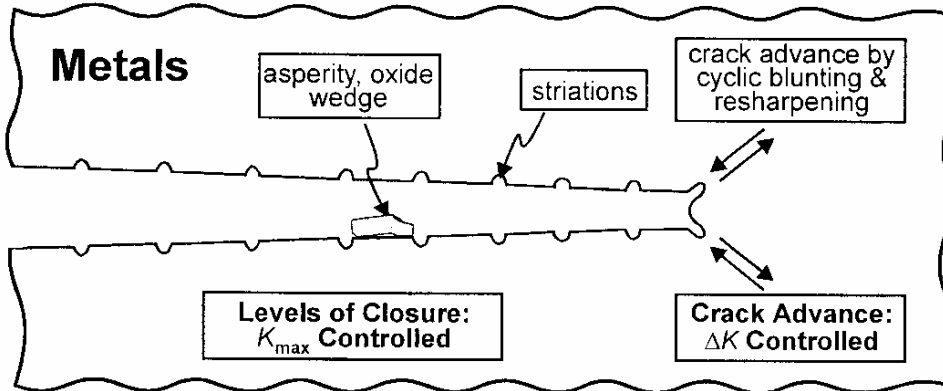
500 nm

Traditional Fatigue Mechanisms

Bulk ductile materials

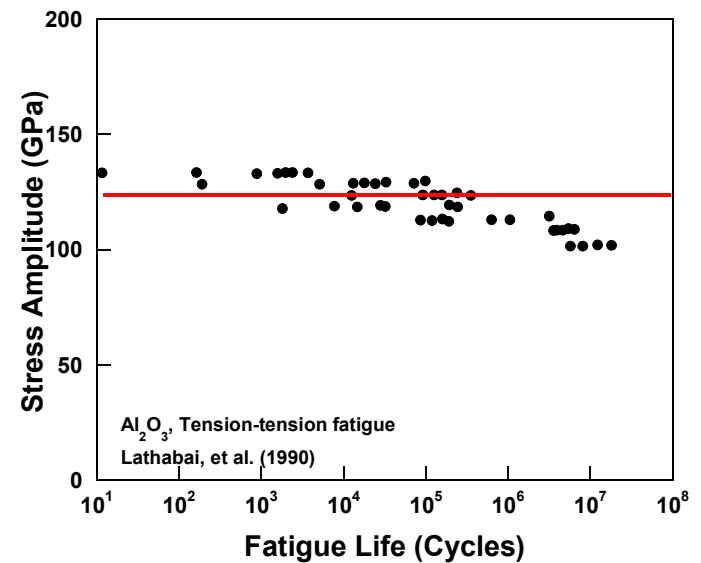
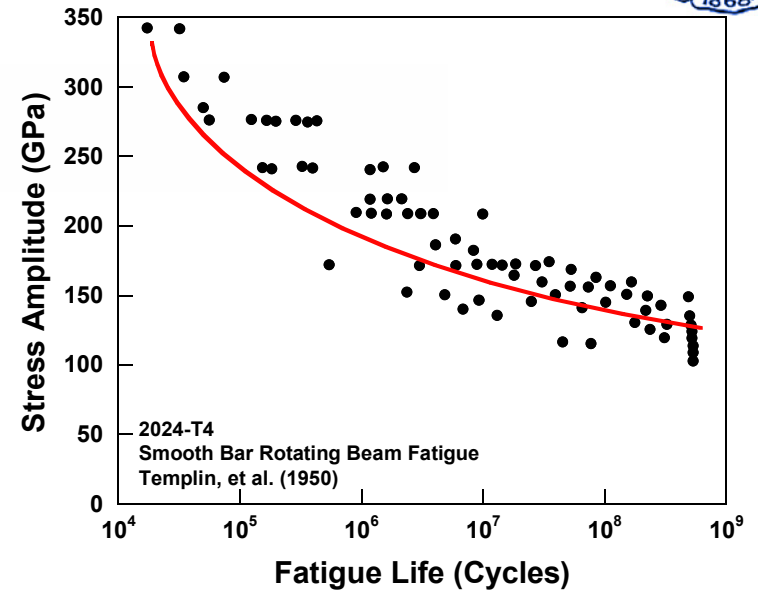
Extrinsic Processes

Intrinsic Processes



(Ritchie, 1989)

Bulk brittle materials



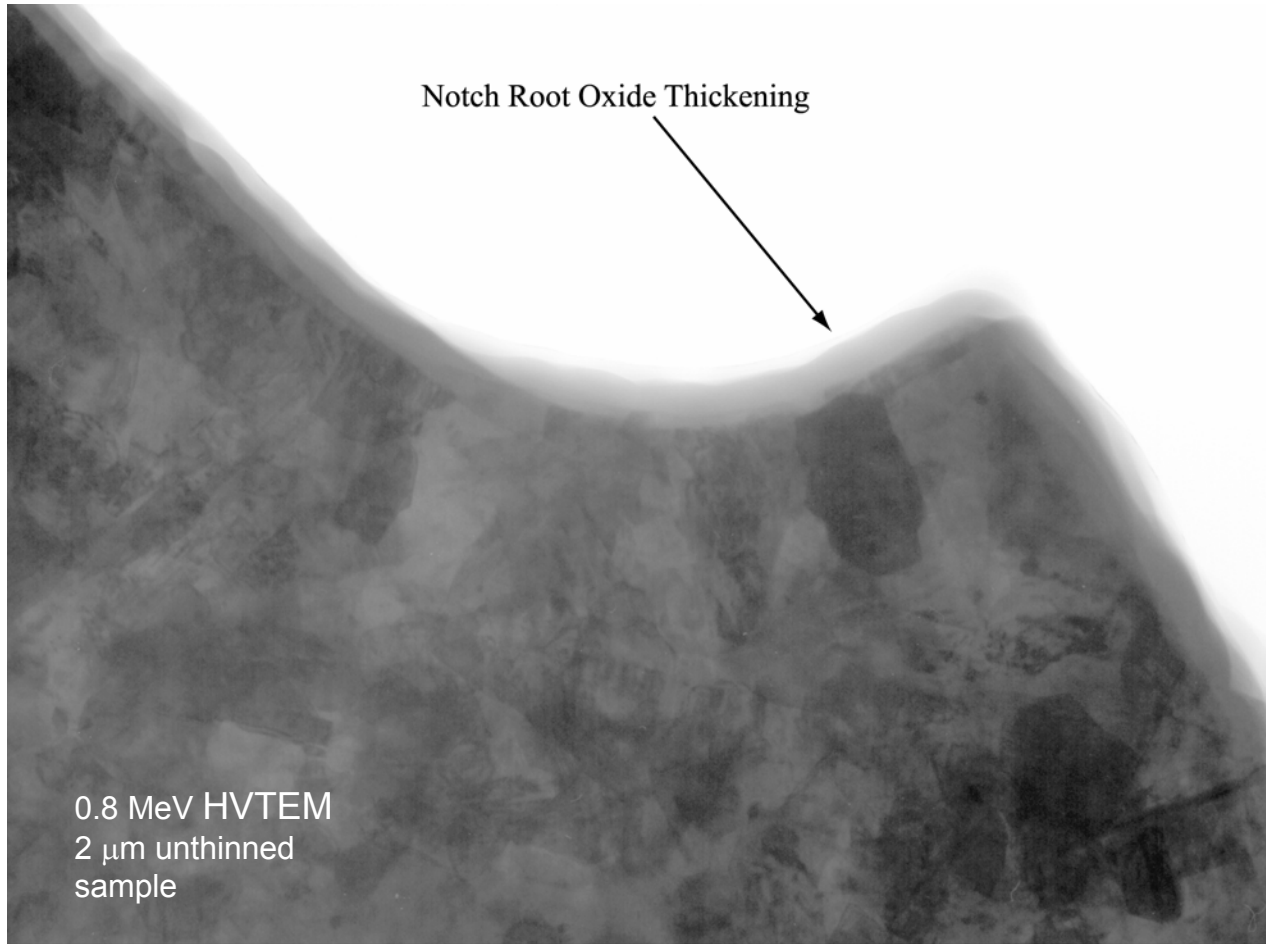


Proposed Mechanisms of Silicon Fatigue



- **Dislocation activity in thin films**
- **Stress-induced phase transformations (e.g., amorphous Si)**
- **Impurity effects (e.g., precipitates)**
- **Suppression of crack-tip shielding**
- **Surface effects (native oxide layer)**

Notch Root Oxide Thickening

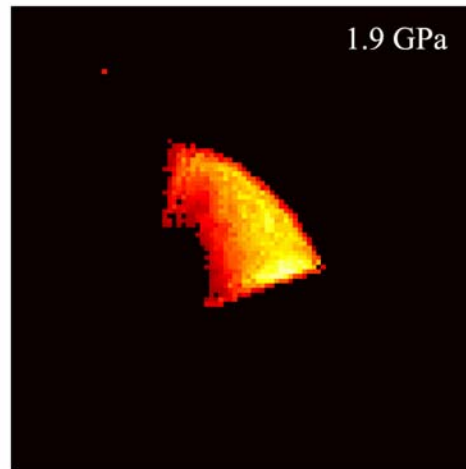
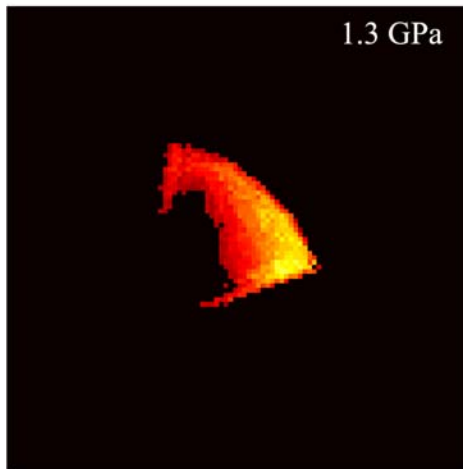
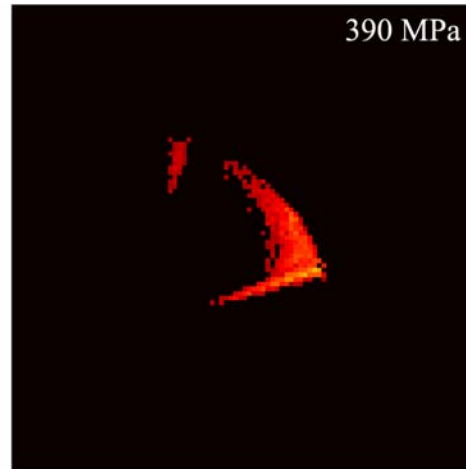
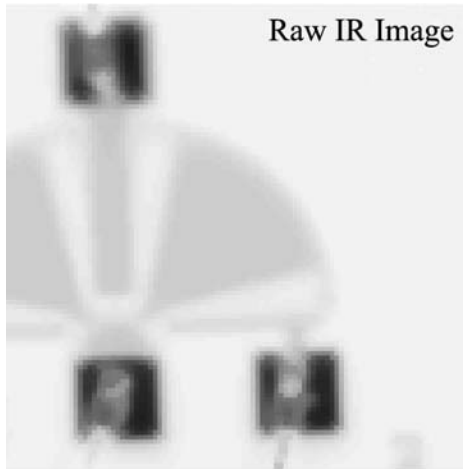


- native oxide thickness ~ 30 nm
- *in fatigue*, oxide thickness at notch root seen to thicken three-fold to ~ 100 nm
- *in sustained loading*, no such thickening is seen

500 nm

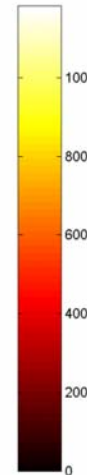
$$\sigma_a = 2.26 \text{ GPa}, N_f = 3.56 \times 10^9 \text{ cycles}$$

Thermal vs. Mechanical Oxide Thickening



300 μm

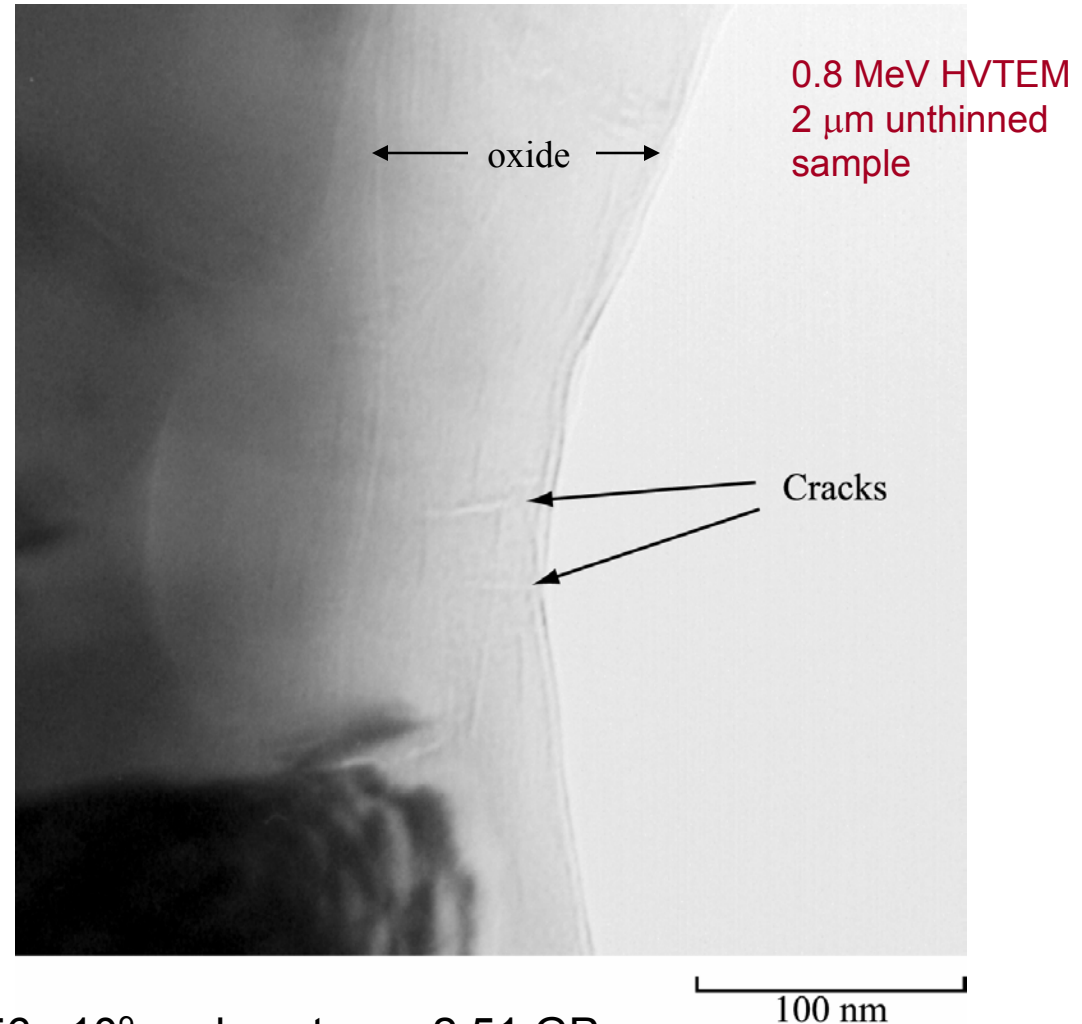
<1K



- temperature measured *in situ* at various stresses using a high-resolution IR camera
- IR camera capable of detecting ΔT to within mK with lateral positioning within microns
- small changes in ΔT of the resonant mass due to friction with the air
- notch region shows no change (<1 K) in ΔT during the fatigue test
- *the observed 3-fold thickening of the oxide film in the notch region is promoted by mechanical rather than thermal factors*

Crack Initiation in Notch Root Oxide

- crack initiation in oxide scale during interrupted fatigue test
- evidence of several cracks ~40 – 50 nm in length
- length of cracks consistent with change in resonant frequency
- strongly suggests subcritical cracking in the oxide layer, consistent with proposed model for fatigue



interrupted after 3.56×10^9 cycles at $\sigma_a = 2.51$ GPa



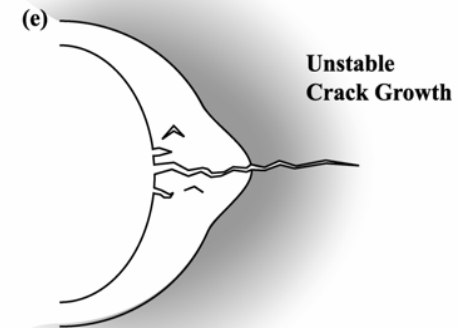
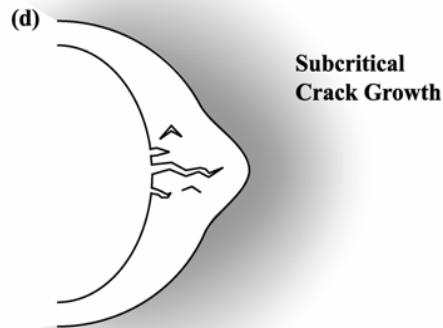
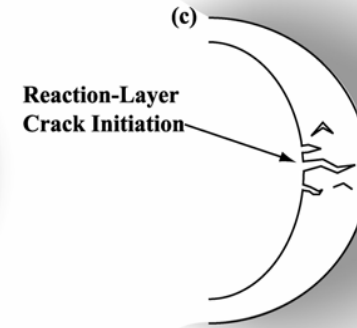
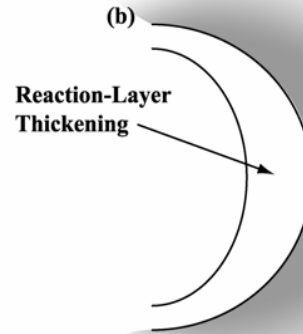
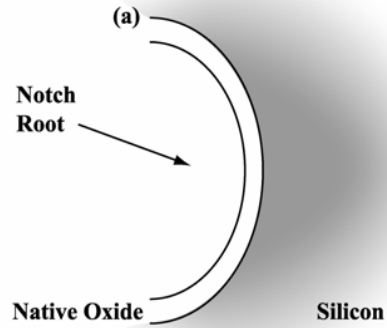
Relative Crack-Growth Resistance of Si and SiO₂



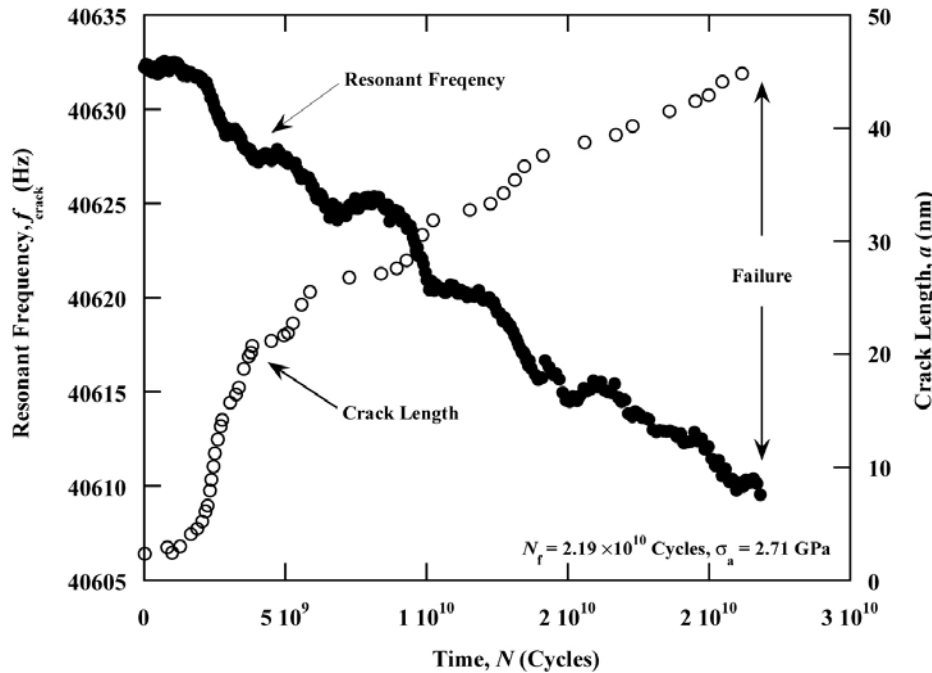
- Progressive time/cycle dependent fatigue mechanism could involve an alternating process of *oxide formation* and *oxide cracking*. However, the fracture toughnesses of Si and SiO₂ are comparable:
 - Si: $K_c \sim 1 \text{ MPa}\sqrt{\text{m}}$
 - SiO₂: $K_c \sim 0.8 - 1 \text{ MPa}\sqrt{\text{m}}$
- In contrast, the susceptibility of Si and SiO₂ to *environmentally-assisted cracking* in the presence of moisture are quite different, with silica glass being much more prone to stress-corrosion cracking:
 - Si: $K_{\text{IscC}} \sim 1 \text{ MPa}\sqrt{\text{m}}$ (in moisture)
 - SiO₂: $K_{\text{IscC}} \sim 0.25 \text{ MPa}\sqrt{\text{m}}$
- Thus, fatigue mechanism is postulated as a sequential process of:
 - mechanically-induced surface oxide thickening
 - environmentally-assisted oxide cracking
 - final brittle fracture of silicon



Silicon Fatigue Mechanism - Reaction-Layer Fatigue -

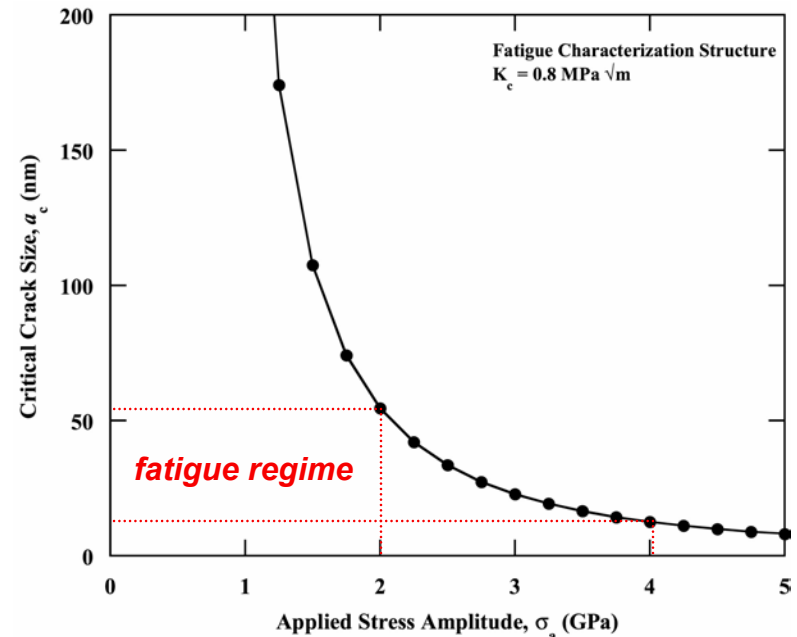


Incipient Cracking during Fatigue Test



- measured change in natural frequency used to compute specimen compliance and hence crack length throughout the test
- for $\sigma_a = 2 - 5$ GPa, crack lengths at onset of specimen failure remain less than ~ 50 nm

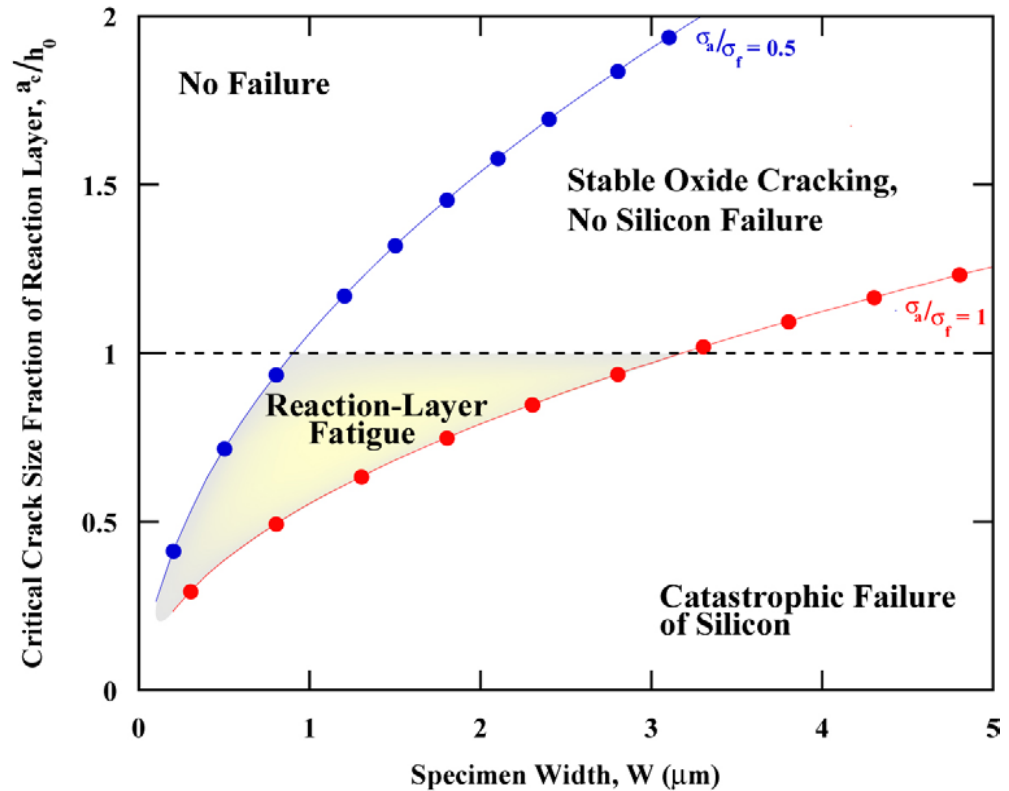
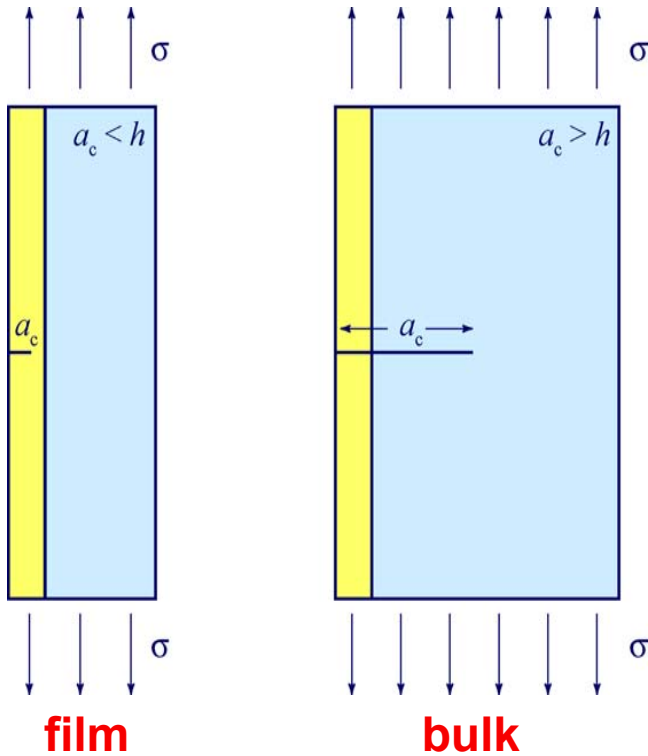
$$K_C = Q \sigma_F (\pi a_C)^{1/2}$$



- this suggests that the entire fatigue process, i.e.,
 - crack initiation
 - subcritical crack growth
 - onset of final failure

occurs within the native oxide layer

Why is Only Thin-Film Silicon Susceptible to Reaction-Layer Fatigue?



- mechanism is active for thin-film and bulk silicon in moist air
- due to low surface-to-volume ratio of bulk materials, the effect is insignificant
- critical crack size for failure can be reached in the oxide layer only for thin-film silicon, i.e., where $a_c < h$



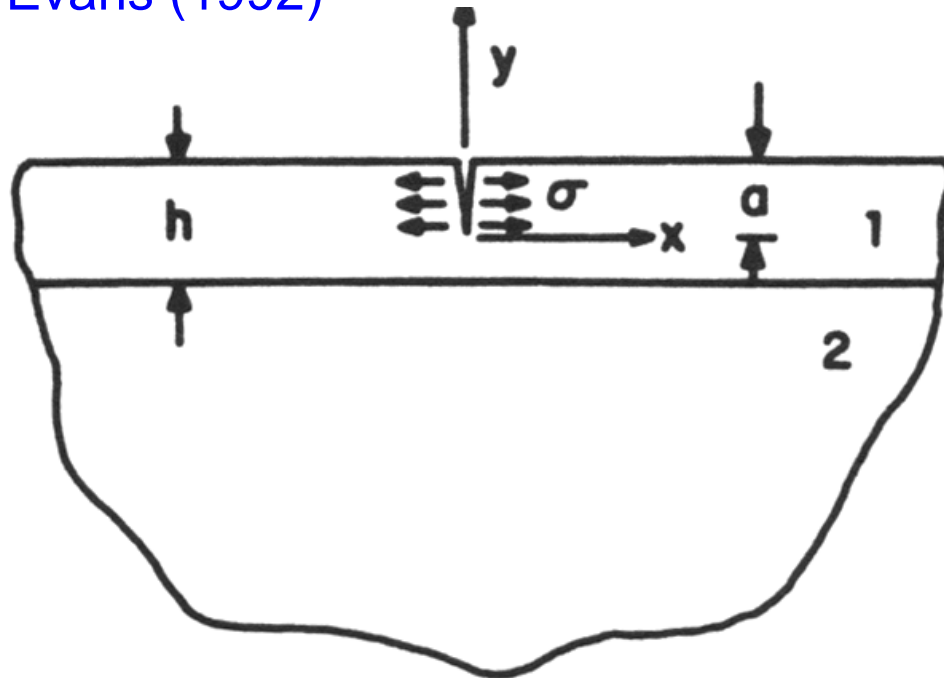
Interfacial Crack Solutions: Crack Inside Layer, Normal to Interface



- Beuth (1992)
 - extension of Civilek (1985) and Suo and Hutchinson (1989,1990)
 - dislocation-based fracture mechanics solution
- Ye, Suo, and Evans (1992)

$$\alpha = \frac{\bar{E}_1 - \bar{E}_2}{\bar{E}_1 + \bar{E}_2}$$

$$\beta = \frac{\mu_1(1-2\nu_2) - \mu_2(1-2\nu_1)}{2\mu_1(1-\nu_2) + 2\mu_2(1-\nu_1)}$$

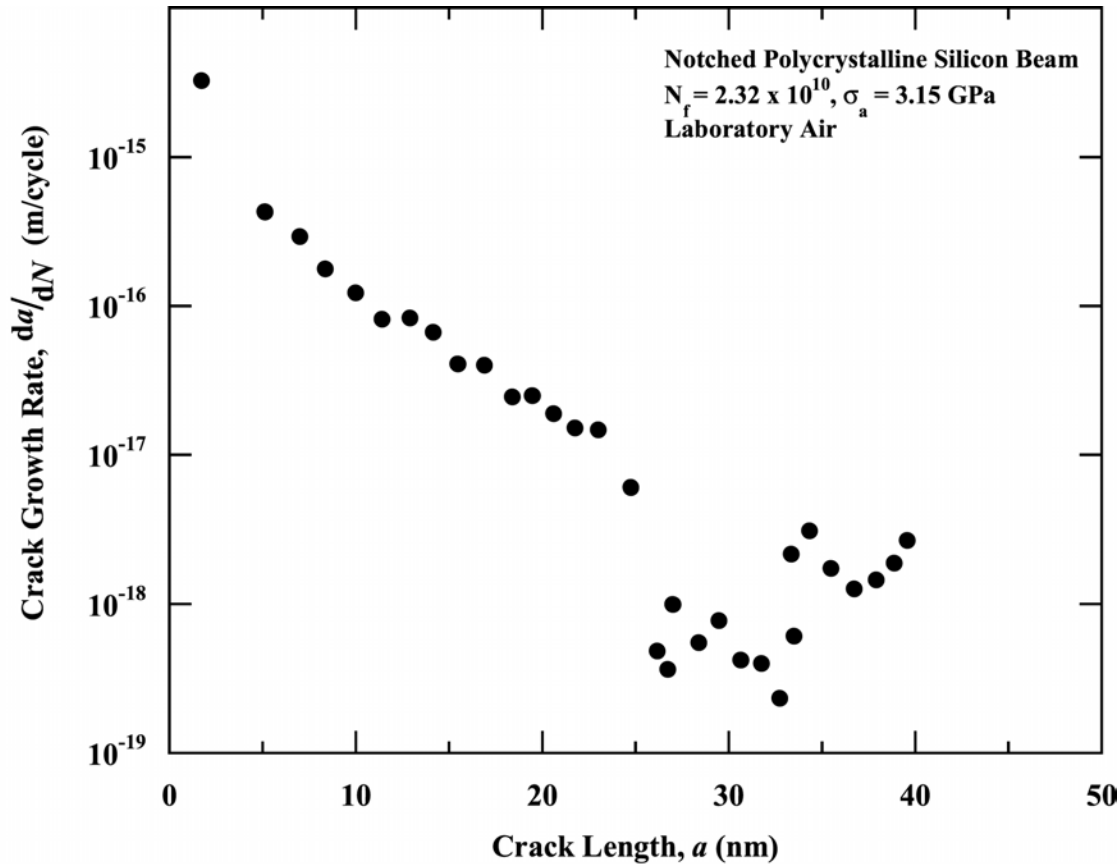


SiO₂/Si

$$\alpha = -0.5$$

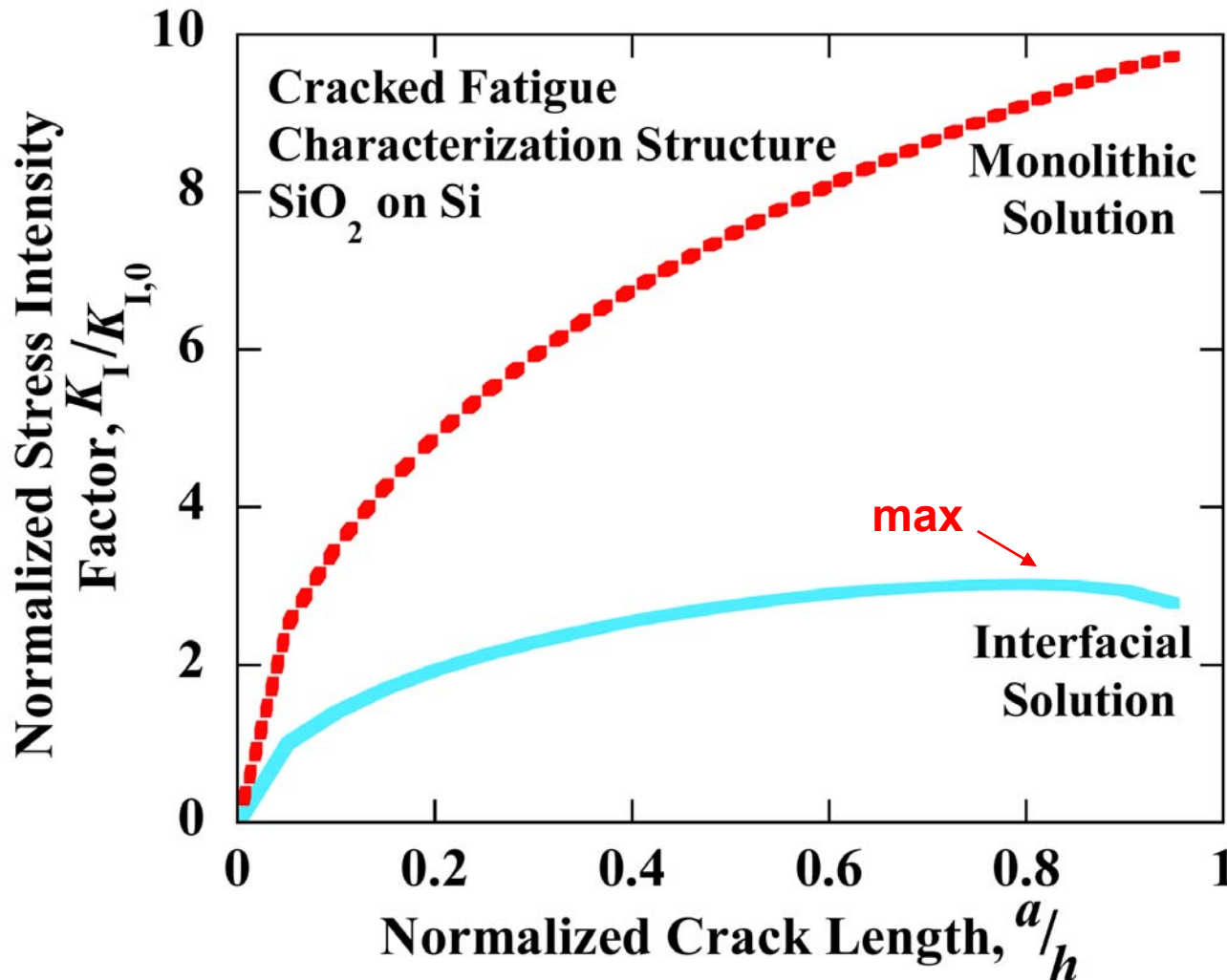
$$\beta = -0.2$$

Crack-Growth Rates and Final Failure



- estimated cracking rates display decreasing growth-rate behavior, consistent with:
 - small-crack effects
 - displacement-control conditions
 - residual stresses in film
 - growth toward SiO_2/Si interface

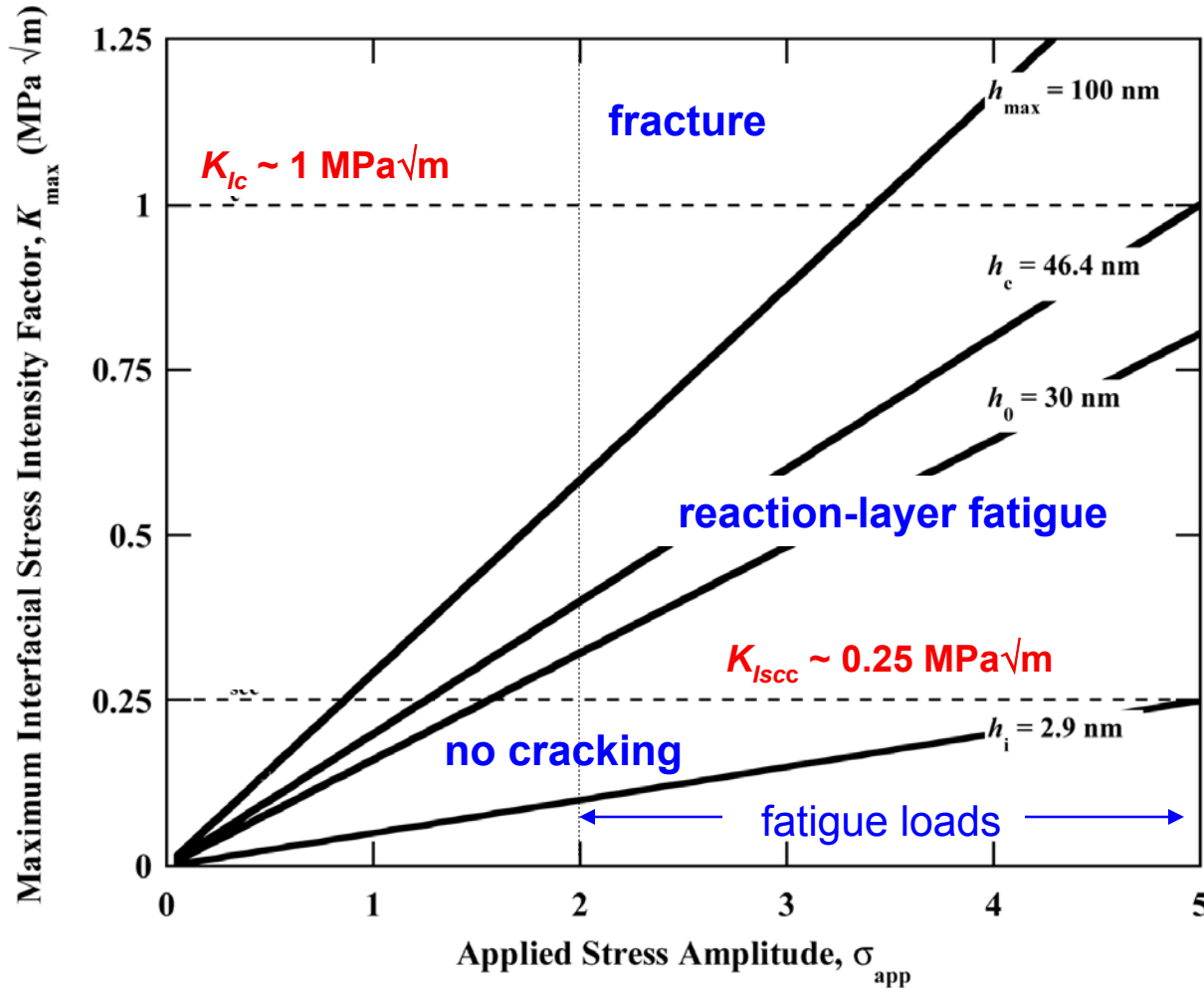
Solution for Crack in Native Oxide of Si



- interfacial solutions for a compliant (cracked) SiO_2 layer on a stiff silicon substrate
- crack-driving force K is $f(a, h)$
- *maximum* K is found at $a_c/h \sim 0.8$

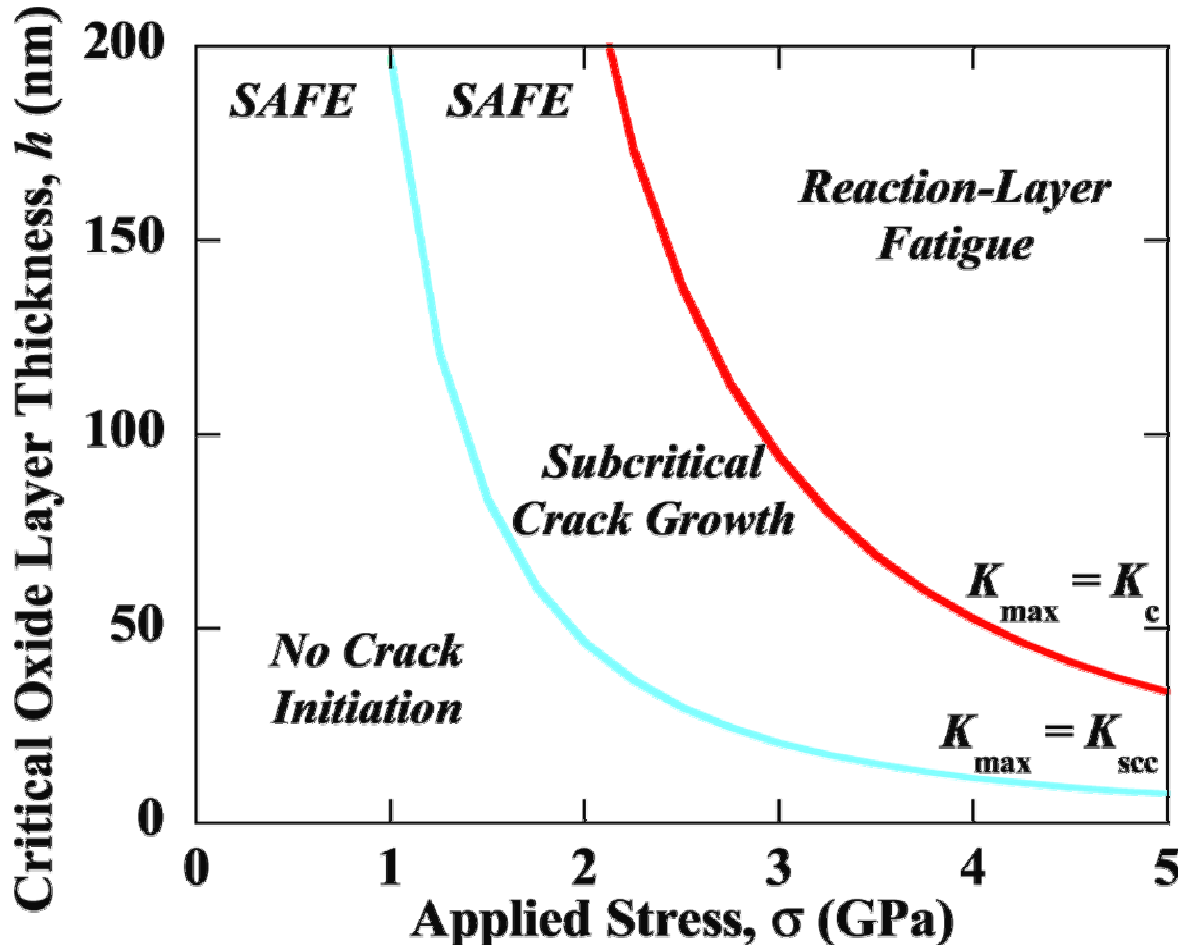
$K_{I,0}$ is the interfacial K where $a/h = 0.05$; $h = 100$ nm

Interfacial Crack-Driving Force



- maximum K at $(a/h) \sim 0.8$
- in range of fatigue failure, where $\sigma_{\text{app}} \sim 2$ to 5 GPa, cyclic-induced oxidation *required* for reaction-layer fatigue
- oxide thickness ≥ 46 nm for failure at $\sigma_{\text{app}} < 5$ GPa
- oxide thickness ≥ 2.9 nm for crack initiation at $\sigma_{\text{app}} < 5$ GPa

Bounds for Reaction-Layer Fatigue

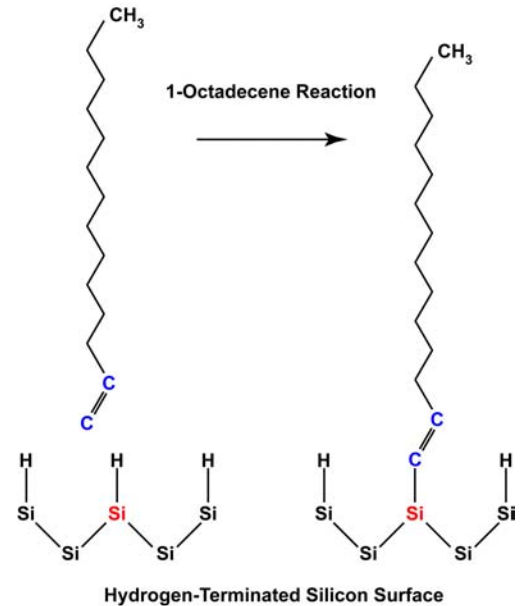
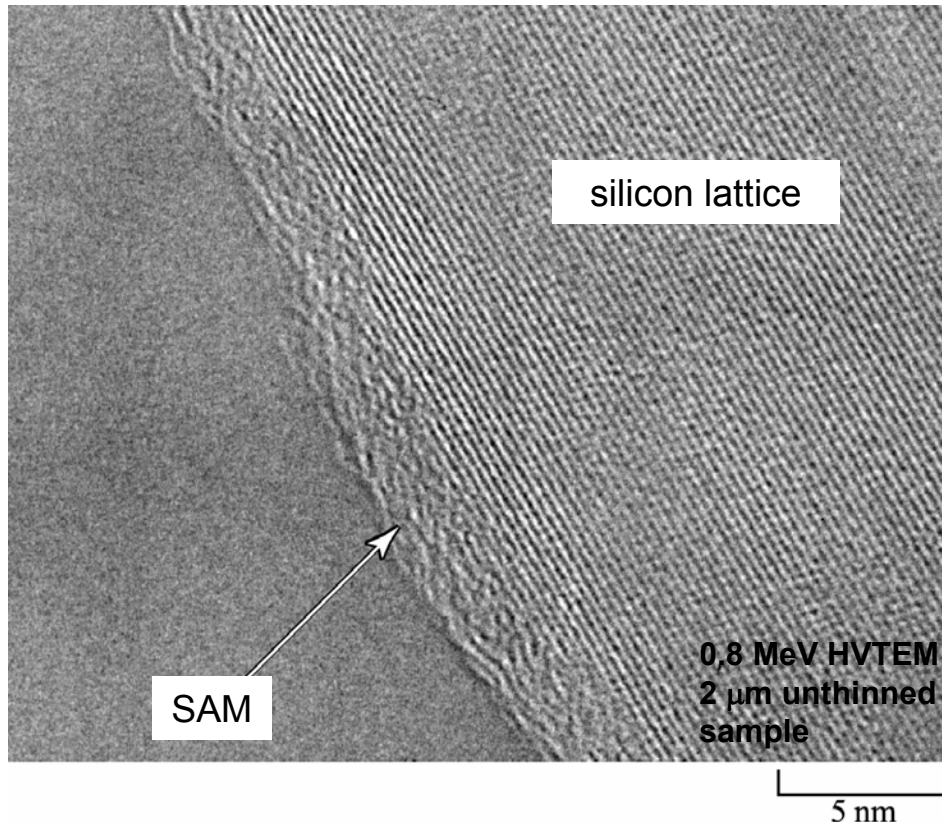


- behavior dependent on reaction-layer thickness
- bounds set by K_{IscC} and K_c of the oxide
- regimes consist of:
 - no crack initiation in oxide ($K < K_{\text{IscC}}$)
 - cracking in oxide but no failure ($K_{\text{IscC}} < K < K_c$)
 - reaction-layer fatigue ($K > K_c$)

- *Reaction-layer fatigue* provides a mechanism for delayed failure in thin films of materials that are ostensibly immune to stress corrosion and fatigue in their bulk form

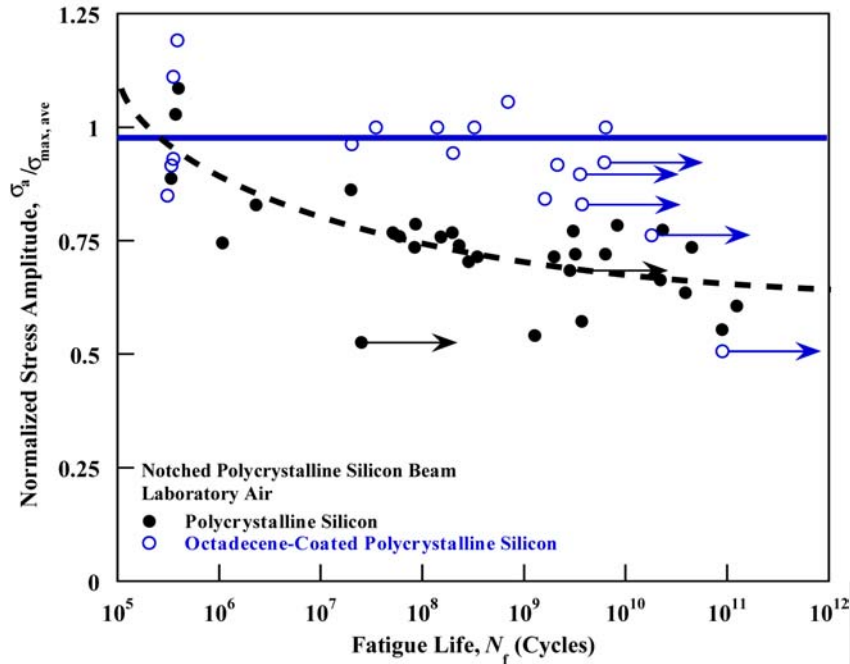
Alkene-Based Self-Assembled Monolayer Coatings

- fatigue testing in the absence of oxide formation achieved through the application of alkene-based monolayer coatings



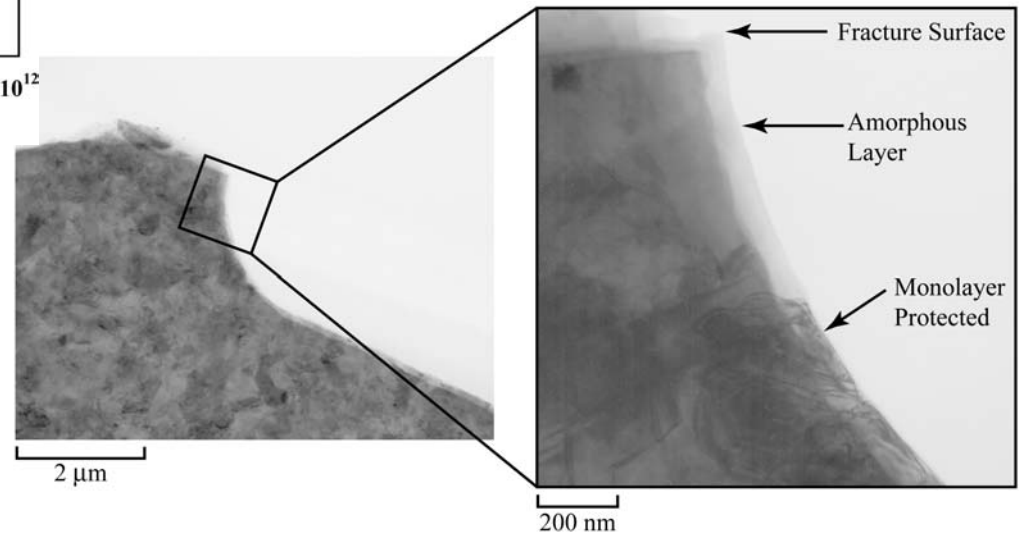
- Si chip is dipped in HF and then coated with alkene-based monolayer coating – *1-octadecene*
- alkene-based coating bonds directly to the H-terminated silicon surface
- coating is a few nm thick, hydrophobic, and stable up to 400°C; *providing a surface barrier to moisture and oxygen*

Suppression of Reaction-Layer Fatigue



- SAM-coated Si samples display far reduced susceptibility to cyclic fatigue
- absence of oxide formation acts to prevent premature fatigue in Si-films

- alkene-based SAM coatings, however, do lower the fracture strength
- oxidation during release smooths out surface; with coatings, sharp surface features remain





Conclusions



- Below a ductile-brittle transition temperature of $\sim 500^\circ\text{C}$, Si displays a high fracture strength (1 - 20 GPa in mono- and 3 - 5 GPa in poly-crystalline Si)
- However, Si is intrinsically brittle with a fracture toughness of $\sim 1 \text{ MPa}\sqrt{\text{m}}$ (approximately twice that of window pane glass!). This value is independent of microstructure and dopant type
- Evaluation of probability of fracture can be made using weakest-link statistics and/or nanoscale crack detection
- Thin film (micron-scale) Si is susceptible to delayed fracture under sustained and particularly high-cycle fatigue loading - premature failure can occur in room air at $\sim 50\%$ of the fracture strength
- Mechanism of cyclic fatigue is associated with mechanically-induced thickening and moisture-induced cracking of the native oxide (SiO_2) layer
- Mechanism significant in thin-film (and not bulk) Si as the critical crack sizes for device failure are less than native oxide thickness, *i.e.*, $a_c < h_{\text{oxide}}$
- Suppression of oxide formation at the notch root, using alkene-based SAM coatings, markedly reduces the susceptibility of thin-film silicon to fatigue.



Bottom line: What affects fracture in silicon?



• Brittle Fracture

- Si-Si bond rupture
- defect (crack) population
- residual stresses

Probability of fracture depends on defect (crack) population

- smooth surfaces, round-off edges, etch out cracks
- use weakest-link statistics
- detect microcracks on the scale of tens of nanometers

• Delayed Fracture

- cracking in native oxide layer (thin film silicon)

