

Mills 1 in class F 2/17 wk 5
 M1 from 2 in class extended 3:10-4:30
 F 3/24 wk 10

See me if that's a problem

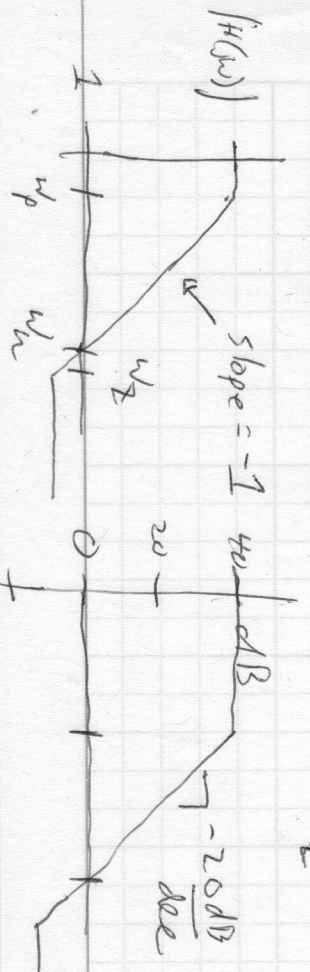
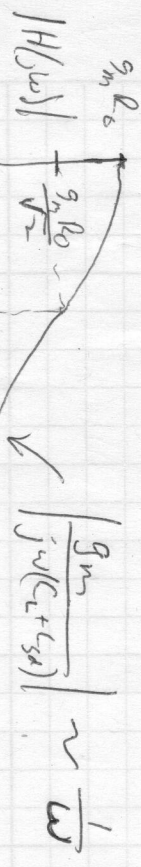
More room to carry if possible??

Single pole amps

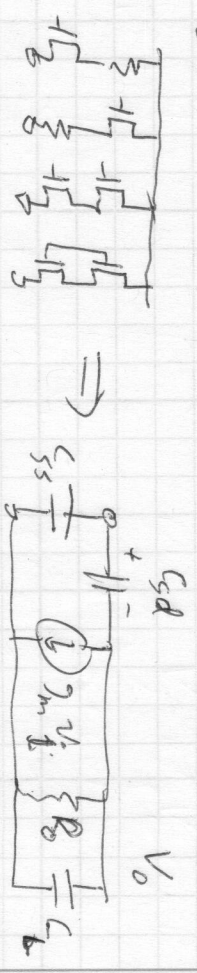
CMOS C.S.

$$\omega_P = \frac{1}{R_o(C_L + C_{gd})}$$

$$\omega_Z = \frac{g_m}{C_{gd}} \text{ in R.H.P.}$$



C.S



Write down KCL @ V_o

$$g_m v_i + \frac{1}{R_o} v_o + s C_{L0} v_o + s C_{gd} (v_o - v_i) = 0$$

$$v_o \left(\frac{1}{R_o} + s(C_L + C_{gd}) \right) = -g_m v_i + v_i (g_m - s C_{gd})$$

$$\frac{v_o}{v_i} = \frac{-g_m - s C_{gd}}{\frac{1}{R_o} + s(C_L + C_{gd})} = -g_m R_o \frac{1 - s/\omega_z}{1 + s/\omega_p} = H(s)$$

effect of

increasing R_o

Avo ↑ ω_p ↓
 by same amount

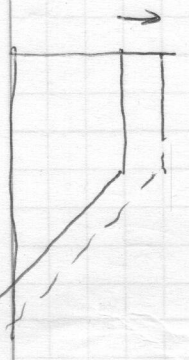
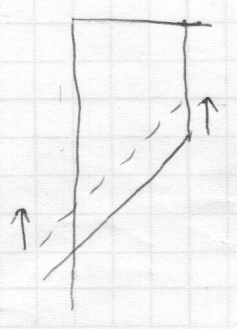
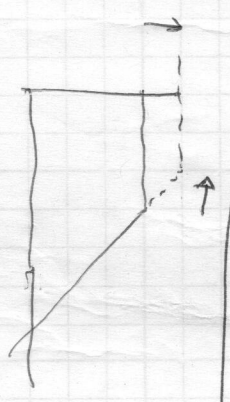
increase C_L

ω_p ↓ ω_z ↓

increase g_m

Avo ↑ ω_z ↑

speed ↑



140/240A 17BP W3L3

$$A_{vo} = g_m R_o$$

$$\omega_p = \frac{1}{R_o (C_L + C_{s,d})}$$

$$\omega_u = \frac{g_m}{C_L + C_{s,d}}$$

must have that

$$A_{vo} \omega_p = \omega_u \quad (\text{slope} = -1)$$

$$(g_m R_o) \left(\frac{1}{R_o (C_L + C_{s,d})} \right) = \frac{g_m}{C_L + C_{s,d}} = \omega_u$$

check!

for single pole

$$A_{vo} \quad \omega_p \quad \omega_u$$

pick any 2

{ any 2 }

+ { any 1 } \Rightarrow Fully Specified

$$g_m \quad R_o \quad C_L$$

independent, but...

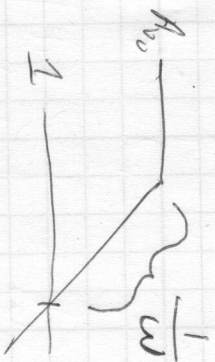
I love this table on midterm 1 (prob 4 on HW)

for single pole

if $1 < A < A_{vo}$

then knowing (A, ω_p)

gives $\omega_u = A \omega_p$



ω_u, C_L place a lower limit on currents

$$\omega_u = \frac{g_m}{C_L}$$

need $g_m \geq \omega_u C_L$

$$g_m = \frac{I_D}{nV_T} \quad \text{best case} \quad \text{SO} \quad I_D \geq nV_T \omega_u C_L$$

$$(A_{vo}, \omega_p, \omega_u) \leftrightarrow (g_m, R_o, C_L) \leftrightarrow I_D, W, L, V_{ov}$$

$$I_D = \frac{\mu_n C_{ox}}{2} \frac{W}{L} (V_{gs} - V_{th})^2 (1 + \lambda V_{ds})$$

PROCESS Variables (choose from small set)

design variables

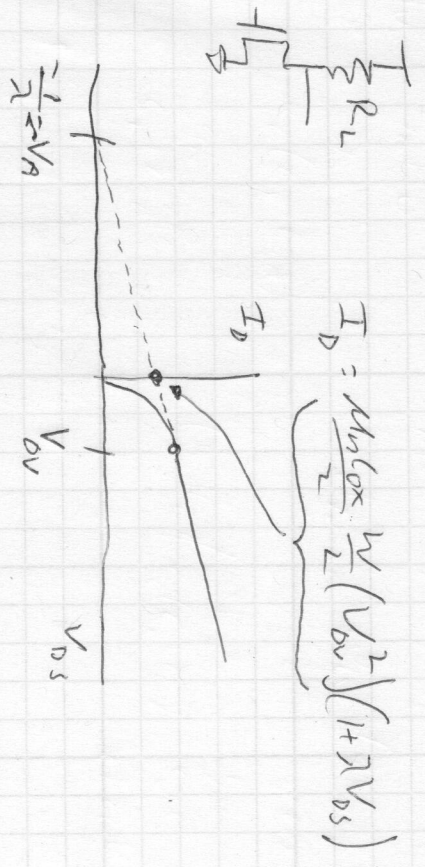
$$g_m = \frac{2 I_D}{V_{ov}} = \mu_n C_{ox} \frac{W}{L} V_{ov}$$

$$R_o = \frac{(1 + \lambda V_{ds})}{\lambda I_D}$$

$$(g_m, R_o, C_{par}) \leftrightarrow (I_D, \frac{W}{L}, V_{ov}, L)$$

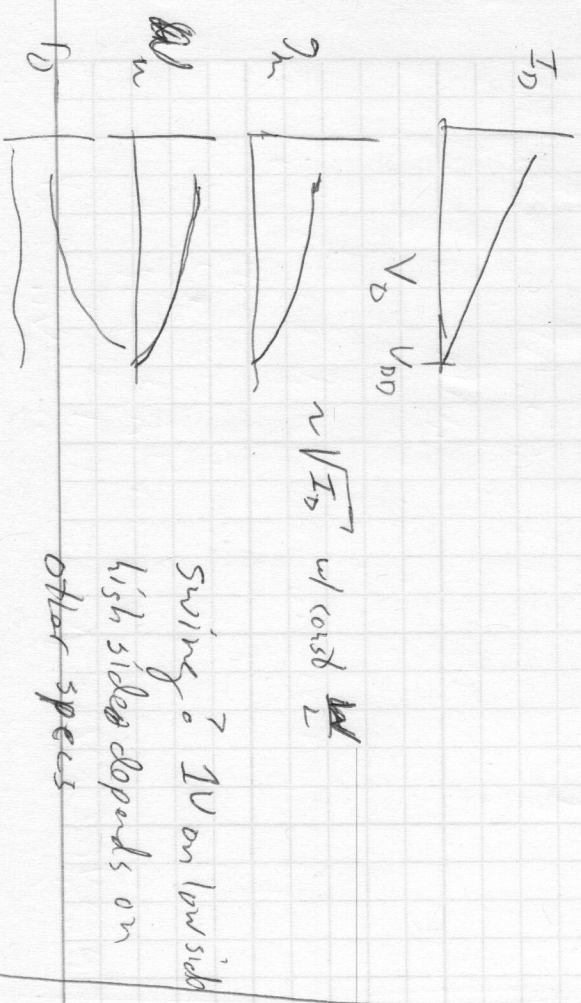
Choose any 2

Why CMOS CS?



$$I_D = \frac{\mu_n C_{ox}}{2} \left(\frac{W}{L} \right)^2 (V_{ov}^2) (1 + \lambda V_{ds})$$

What about $(I_D, g_m) \Rightarrow (A_{vo}, w_p, w_s)$
 look like vs. V_{DD} ?



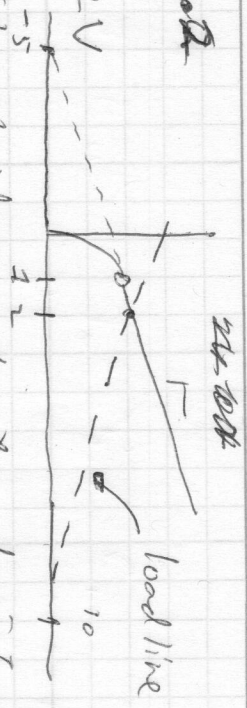
$$\sim \sqrt{I_D} \text{ w/ const } W$$

Swing? $\sim 1V$ on low side
 high sides depends on
 other specs

say $\lambda = 0.02$

$$V_{ov} = 1V$$

$$V_{ds} = 2V$$



What resistor should I use to get good gain?

Ideally $R_L > r_D$, so we need $V_{DD} > 2 + 7 = 9V$

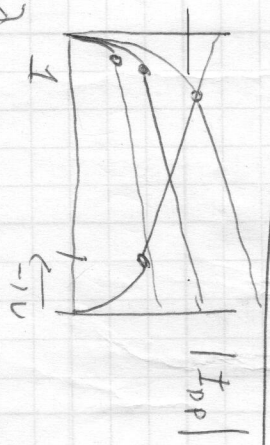
What if $V_{DD} = 5V$?

can't get that R_L at that current.

if $V_{DD} < \frac{1}{\lambda} R_L$ R_L always $< r_D$

CMOS

$$V_{ov} = \sqrt{\frac{I_D}{\mu_n C_{ox} \left(\frac{W}{L} \right)^2}}$$



$r_{op} = r_{on}$ if $\lambda_p = \lambda_n$
 current still not constant but less variation

A_{vo}, w_p, w_s roughly constant over output swing
 which is $[V_{ov}, V_{DD} - |V_{ovp}|]$

current varies less than $\frac{\partial I_D}{\partial V_{DD}}$

Why not make $L_p \gg L_n$? (so that $\lambda_p \ll \lambda_n$)

OK up to pt where C_{gd} affects performance