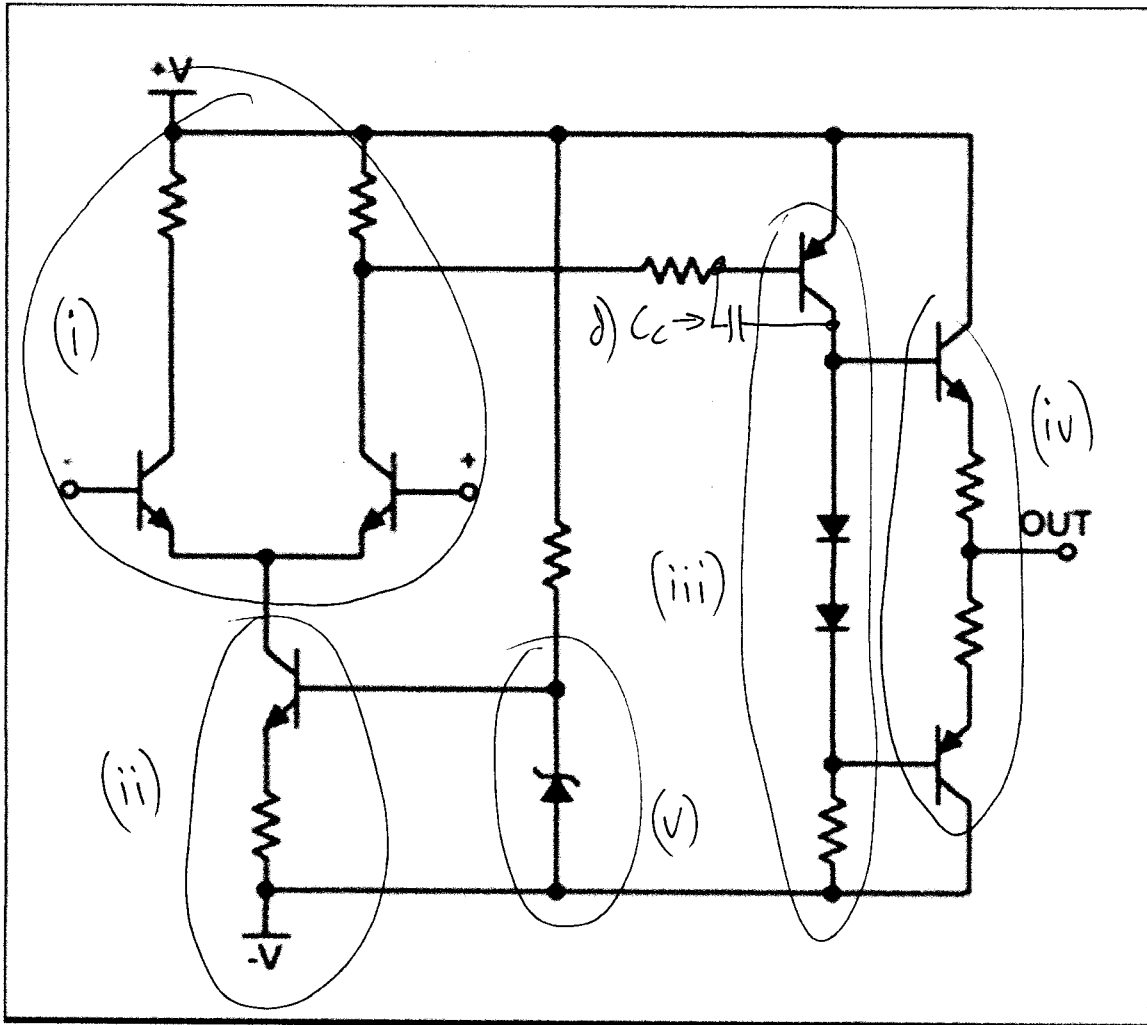


EE140 HW 6 Solutions

1) a)



b) The resistor limits the current in that branch.

c) $I_{tail} = (3.5V - 0.7V - V_-) / 1 \text{ kohm} = 2.8 \text{ mA}$ (assuming $V_- = 0V$)

The Zener voltage is relatively constant regardless of supply variation so I_{tail} is mostly independent of the supply voltage.

d) See above.

#1) 9 pts total

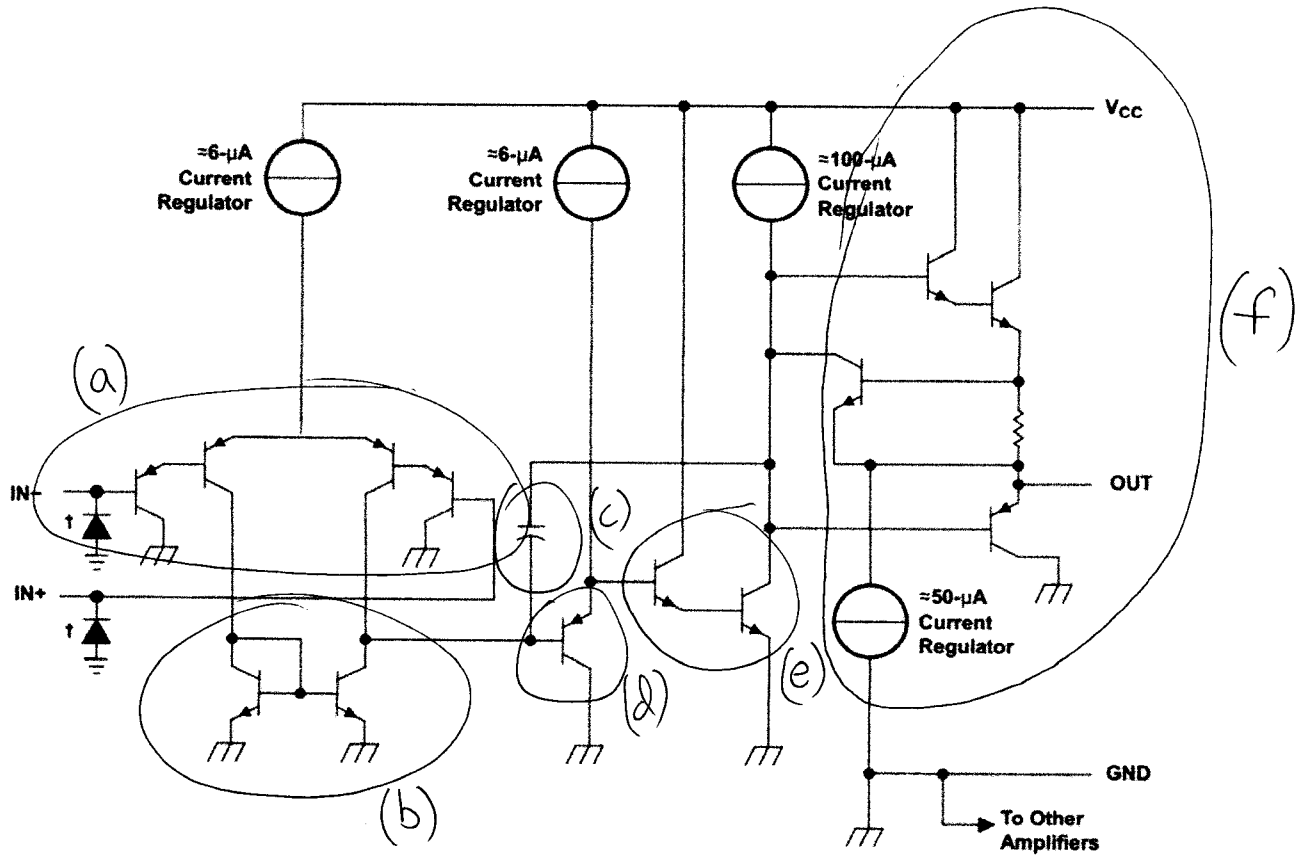
a) 5 pts, 1 for identifying each block

b) 1 pt

c) 2 pts, 1 for tail current, 1 for supply variation comment

d) 1 pt

2)



#2) 6 pts total
1 pt each for identifying each block

3)

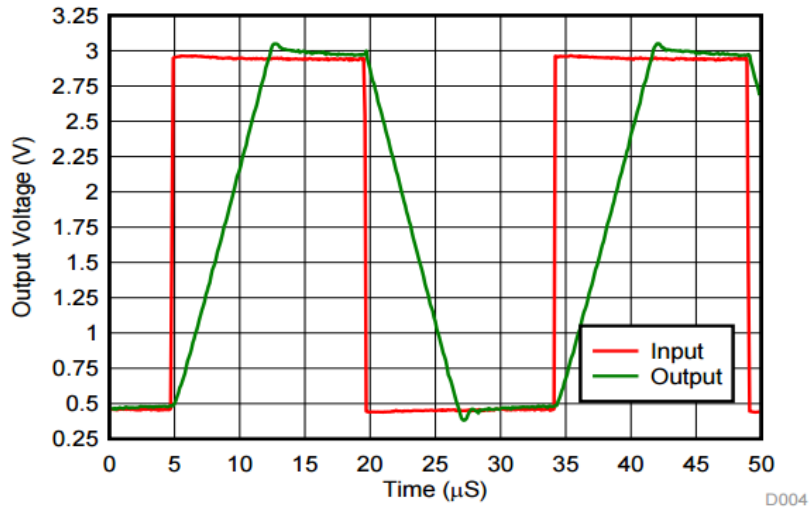


Figure 4. Voltage Follower Large Signal Response (50 pF)

- The rising slew rate is $1.75\text{V}/5\mu\text{s} = 350\text{ kV/s}$ and the falling is $2\text{V}/5\mu\text{s} = 400\text{ kV/s}$.
- The smallest of all the source/sink values in the table is 1mA , which leads to $dV/dt = I/C = 1\text{mA}/50\text{pF} = 20\text{ MV/s}$. This number is much larger than the slew rate in Fig 4 so the output stage is not the limiting factor.
- The slew rate must then be due to the compensation capacitor, which on both rising and falling edges has a current limit of $6\mu\text{A}$ due to the $6\mu\text{A}$ diff pair current source. $C = I / (dv/dt)$. Taking the average of the rise/fall slew rates, $C = 6\mu\text{A} / (375000\text{ V/s}) = 16\text{ pF}$.

#3) 6 pts total

- 2 pts, 1 each for rising and falling slew rates
- 2 pts, 1 for finding output current limit, 1 for saying it is not output slew limited
- 2 pts, 1 for tail current as limiting factor, 1 for calculating C_c

4)

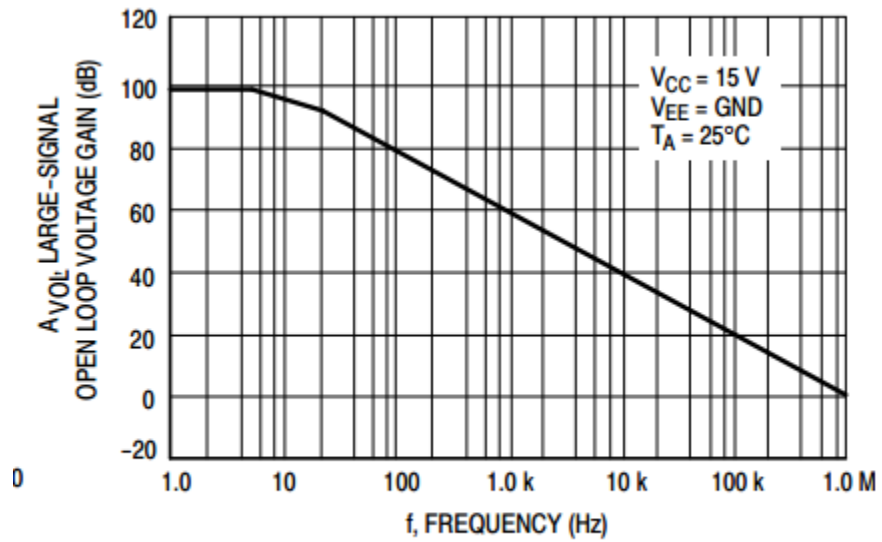


Figure 6. Open Loop Frequency

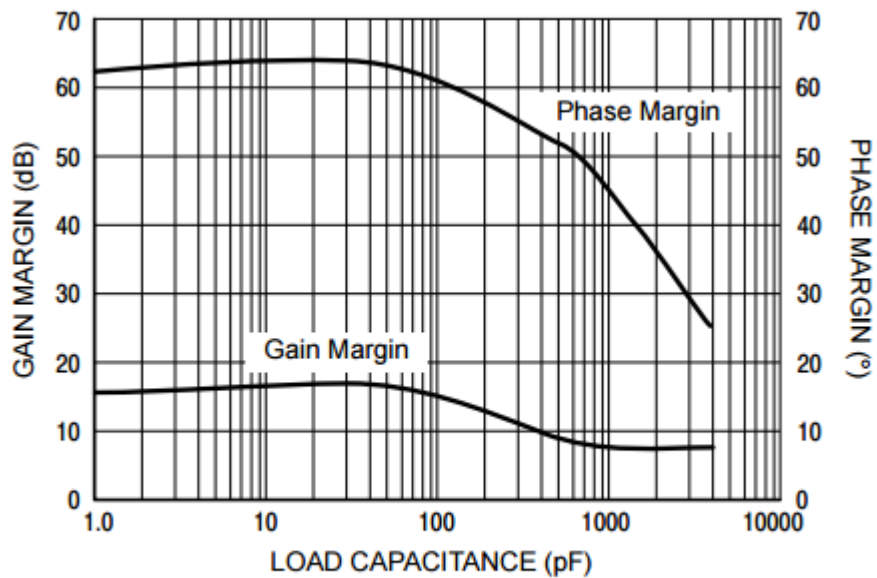


Figure 4. Gain and Phase Margin

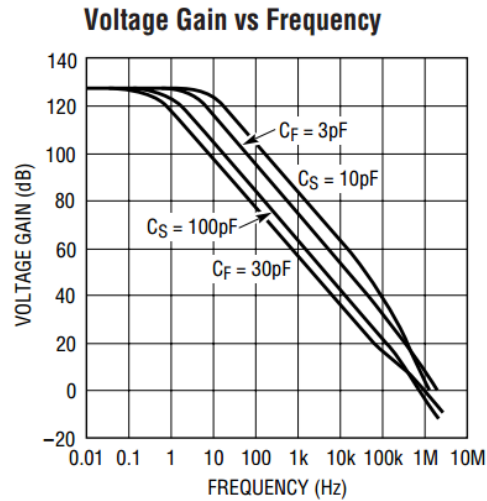
- a) $A_{v0} = 100,000$ V/V, $f_{p1} = 5$ Hz, $f_u = 1$ MHz
- b) The phase margin is 45 degrees for $C_L = 1000$ pF, so P2 must be at the unity gain frequency, $f_{p2} = 1$ MHz.

#4) 5 pts total

a) 3 pts, 1 each A_{v0} , f_{p1} , f_u

b) 2 pts, 1 for saying $PM=45$, 1 for saying $\omega_{p2}=\omega_u$

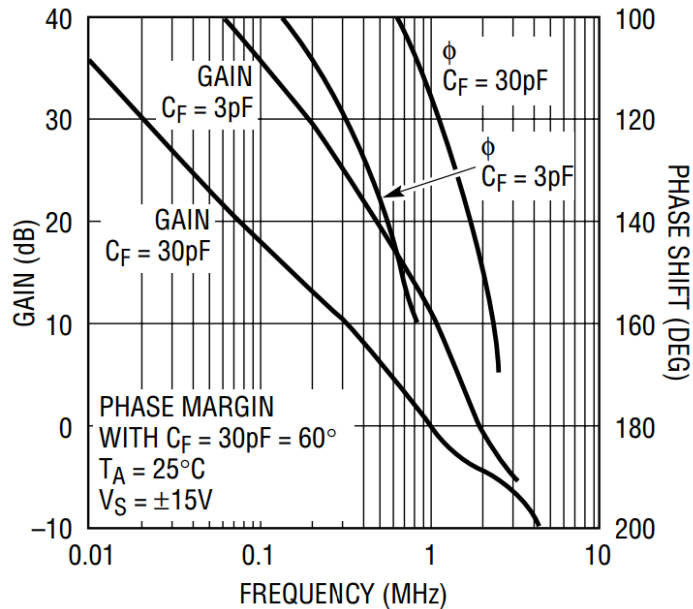
5)



a)

- i. Gain at 0.1Hz is about 3×10^6 . $f = 0.001$, so closed loop gain error is $-1/Af = -1/3000$.
- ii. $C_S = 10\text{pF}$ puts the pole at about 5 Hz, while $C_F = 30\text{pF}$ puts the pole at about 0.2 Hz.

b)



For $PM = 60^\circ$,

$C_F = 3\text{pF}$, the minimum gain is 26dB @ 300kHz (feedback factor of 0.05).

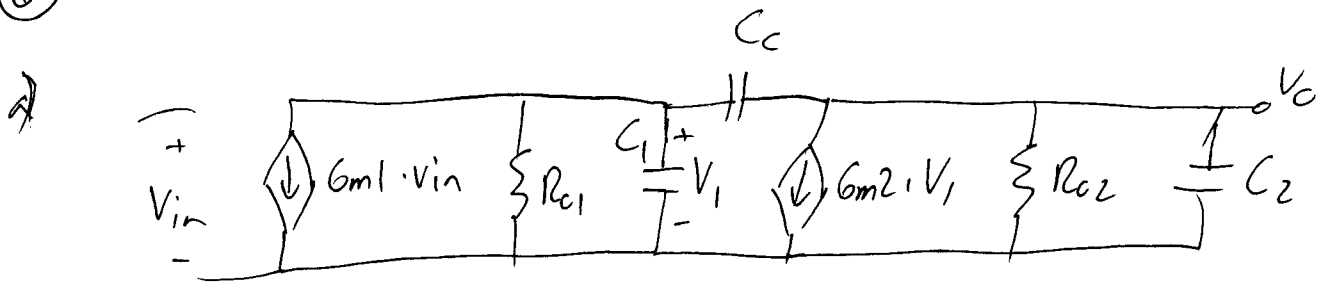
$C_F = 30\text{pF}$, the minimum gain is 0dB @ 1MHz (feedback factor of 1, it is unity gain stable).

#5) 7 pts total

a) 3 pts, 1 for gain error, 1 each for the two poles in (ii)

b) 4 pts, 1 for min gain and 1 for bandwidth, for both values of C_F

6)



b)

$$\frac{V_{out}}{V_{in}}(s) = \frac{(C_c s - G_{m2}) R_{o2}}{R_{o1} R_{o2} \xi s^2 + R_{o1} (1 + G_{m2} R_{o2}) (C_c + C_1) s + R_{o2} (C_c + C_2) s + 1}$$

where $\xi = C_1 C_c + C_1 C_2 + C_c C_2$

c) i)

$$\omega_{p2} = \frac{1}{\omega_{p1}} \cdot \frac{1}{R_{o1} R_{o2} (C_1 C_c + C_1 C_2 + C_c C_2)}$$

ii) $\omega_{p1} = \frac{1}{R_{o1} G_{m2} R_{o2} C_c}$

#6) 7 pts total
 a) 2 pts for correctly redrawing
 b) 2 pts
 c) 3 pts, 1 for each subpart

$$\omega_{p2} = \frac{G_{m2} C_c}{C_1 C_c + C_1 C_2 + C_c C_2}$$

iii) For $PM \geq 45^\circ$, $\omega_{p2} \geq \omega_u = \frac{G_{m1}}{C_c}$

$$\frac{G_{m2}}{G_{m1}} \cdot \frac{C_c^2}{C_1 C_c + C_1 C_2 + C_c C_2} \geq 1$$

#7) 5 pts total (EE240 only)
 a) 2 pts
 b) 3 pts