

SYNCHRONIZATION AND ANTI-SYNCHRONIZATION OF CHUA'S OSCILLATORS VIA A PIECEWISE LINEAR COUPLING CIRCUIT

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ABSTRACT

A chaotic associative memory may be constructed by coupling a network of Chua's circuits via piecewise linear conductances. Synchronization and anti-synchronization states are used to represent binary memory patterns. The chaotic network dynamics enable the memory to wander among patterns which have non-zero correlations with the input pattern. This paper describes two discrete circuits which may be used as the basis for implementing the coupling element as proposed in Jankowski et. al. [1995]. Initial coupling experiments support the proposed design approaches.

1. INTRODUCTION

Chua's circuit is a nonlinear electronic chaotic oscillator. This circuit is easily constructed [1] and has been employed in a variety of applications [2], e.g. communication systems [3]. The chaotic associative memory architecture proposed in [4] uses a network of Chua's oscillators coupled via piecewise linear conductances. To the best of our knowledge this architecture has been studied only through simulation. An electronic implementation of this circuit offers the opportunity to investigate this architecture as a physical system. The only missing piece needed to build this memory is the piecewise linear coupling element. The basis for two designs of this circuit element are presented in this paper. One design has been built and partially tested. Initial experimental coupling results are consistent with the required circuit functionality.

1.1. Associative Memory Architecture

The associative memory architecture under consideration consists of a network of interconnected Chua's oscillators. The parameters of each oscillator are chosen to generate the "double scroll" attractor. The coupling element (described

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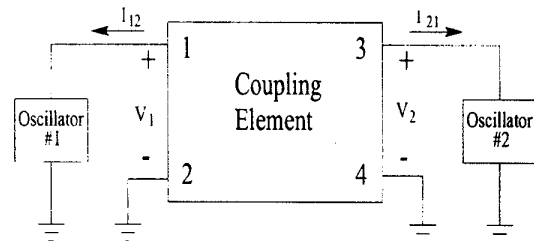


Figure 1: Two coupled Chua's circuits

later) tends to force oscillators to become either synchronized or anti-synchronized. Binary patterns may be stored via specification of the coupling strengths between oscillators as determined by a Hebbian learning rule. Pattern retrieval is accomplished by coupling the input pattern to the network via a master free-running oscillator and observing the temporal response of each of the network oscillators. This response is characterized by temporary synchronization or anti-synchronization states which correspond to the stored patterns. The memory chaotically switches among those pattern memories which possess non-zero correlations with the input pattern. This form of coupling has also been used in a cellular neural network composed of locally coupled Lorenz systems [5].

1.2. Coupling Element Characteristics

In this paper we consider the interconnection of two Chua's oscillators using the coupling element proposed in [4] as shown in Figure 1. If N is the dimension of the stored binary patterns, the architecture requires $N + 1$ oscillators (N for each memory pattern bit plus the master oscillator) coupled via $N(N-1)/2 + N$ coupling elements. Note that N of these coupling circuits are somewhat simplified since the N couplings to the master oscillator do not require both coupling currents (no current flows into the free-running master

oscillator). The coupling currents are [4]¹

$$I_{12} = g_{12} \left[V_2 + \text{sign}(g_{12}) V_1 \left(\left| \frac{V_2}{V_1} \right| - \left| \frac{V_2}{V_1} + \text{sign}(g_{12}) \right| \right) \right]$$

and

$$I_{21} = g_{21} \left[V_1 + \text{sign}(g_{21}) V_2 \left(\left| \frac{V_1}{V_2} \right| - \left| \frac{V_1}{V_2} + \text{sign}(g_{21}) \right| \right) \right].$$

Figure 2 shows I_{12} for $|g_{12}| = 1$. The conductance $g = g_{12} = g_{21}$ determines the slopes of the linear segments and hence the coupling strength. For $g < 0$, $I_{12} = I_{21}$, while for $g > 0$, $I_{12} = -I_{21}$ (not shown). Note that the current is zero when V_1 is synchronized or anti-synchronized with V_2 (i.e. $|V_1| = |V_2|$). We have chosen to couple the voltages across the Chua's diodes in the oscillator circuits.

To illustrate the effect of this coupling element, consider the circuit of Figure 1 for $g < 0$, V_2 held at a constant positive voltage, and oscillator #1 replaced with a capacitor C . Figure 2 ($g < 0$ and $V_2 > 0$ case) indicates that I_{12} is, with the exception of one point, negative for $V_1 > -V_2$. This discharges C and V_1 approaches $-V_2$. For $V_1 < -V_2$, the coupling element provides a positive current, which tends to charge C , and thus V_1 approaches $-V_2$. Hence the element forces $V_1 = -V_2$ as it should for $g < 0$. Note that for V_1 exactly equal to V_2 , the coupling current is zero. This point is unstable as any negative perturbation of V_1 will move V_1 towards $-V_2$. The point $V_1 = -V_2$ is stable for this set of parameters.

2. COUPLING ELEMENT DESIGNS

We now consider two designs for the coupling circuit. First consider I_{12} as shown in Figure 2. The general shape of each of these curves is the same, consisting of (from left to right) a positive, a negative, and a positive resistive region (note the definition of positive current in Figure 1). This characteristic may be generated by using piecewise linear characteristics with adjustable zero-crossing points. Since $I_{12} = \pm I_{21}$, an inverting or non-inverting unity gain current mirror may be used to produce I_{21} from I_{12} .

2.1. Voltage-Based Circuit

Figure 3 shows the block diagram of the coupling circuit for $g < 0$. This circuit requires additional circuitry for the $g > 0$ case. The strategy employed here is to generate an output voltage (V_{o1} and V_{o2}) with the same shape as the desired current characteristics but with slopes of ± 1 . This signal is used to produce the currents via voltage-controlled

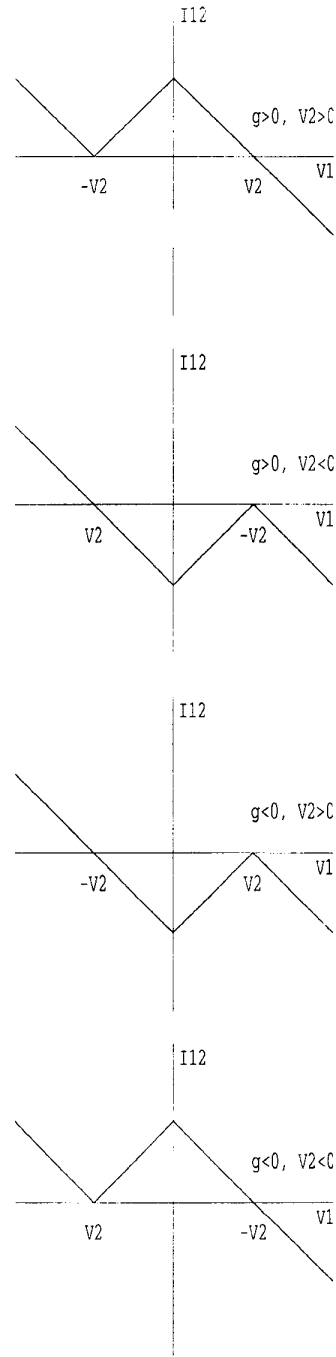


Figure 2: Coupling element current I_{12}

¹ $\text{sign}(x) = -1$ for $x < 0$, 1 otherwise

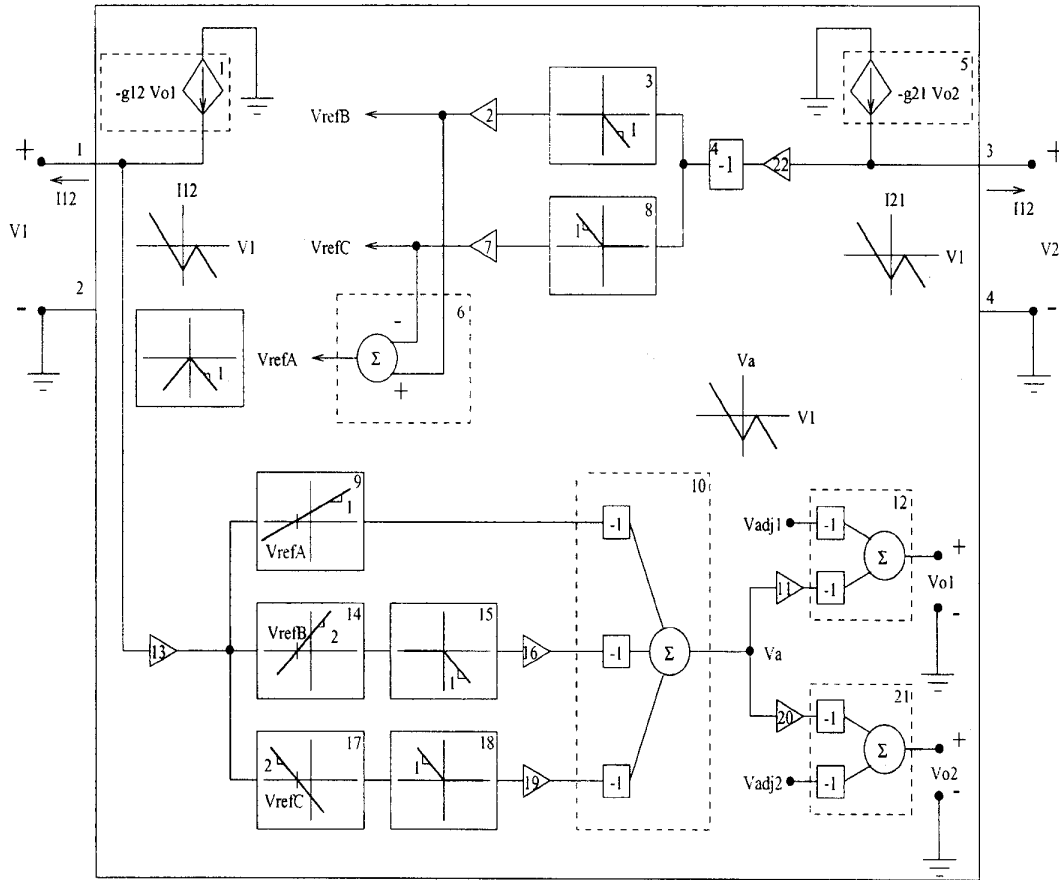


Figure 3: Block diagram of the voltage-based circuit implementation of the negative coupling circuit. Individual operational amplifier circuits are numbered from 1 to 22. Circuit voltage transfer functions are boxed. Non-boxed graphs show transfer functions for the $V_2 > 0$ case.

		V_{refA}	V_{refB}	V_{refC}
$g > 0$	$V_2 > 0$	$-V_2$	$-V_2$	0
	$V_2 < 0$	V_2	0	$-V_2$
$g < 0$	$V_2 > 0$	$-V_2$	0	V_2
	$V_2 < 0$	V_2	V_2	0

Table 1: Required voltage references

current sources. Table 1 indicates the reference voltages required for each stage for both $g > 0$ and $g < 0$. Note that V_2 is processed to produce these reference voltages. The individual circuit elements required are given in Table 2. The voltages V_{adj1} and V_{adj2} adjust the offset of the controlling voltages. Precision 1% resistors, high speed National Semiconductor LM6172 operational amplifiers, and 1N4148 switching diodes are used in this design.

Figure 4 shows experimentally obtained waveforms for coupling two Chua's oscillators with the circuit of Figure 3. The uncoupled case corresponds to (1) removing the connection from the current sources to nodes 1 and 3, (2) connecting the current sources directly to the Chua's circuits, and (3) grounding nodes 1 and 3. This test indicates that the oscillators are not appreciably coupled if the two input voltages to the coupling circuit are equal. The coupled case corresponds to the situation of Figure 1. Note that anti-synchronization is achieved.

2.2. Current-Based Circuit

The second design is based on producing I_{12} and then mirroring the resulting current to generate I_{21} . The basic circuit to generate I_{12} utilizes a parallel combination of several elements described in [8]. These elements are shown in Figure 5. By setting $|g| = 1/R_A = (1/2)R_4/(R_3R) =$

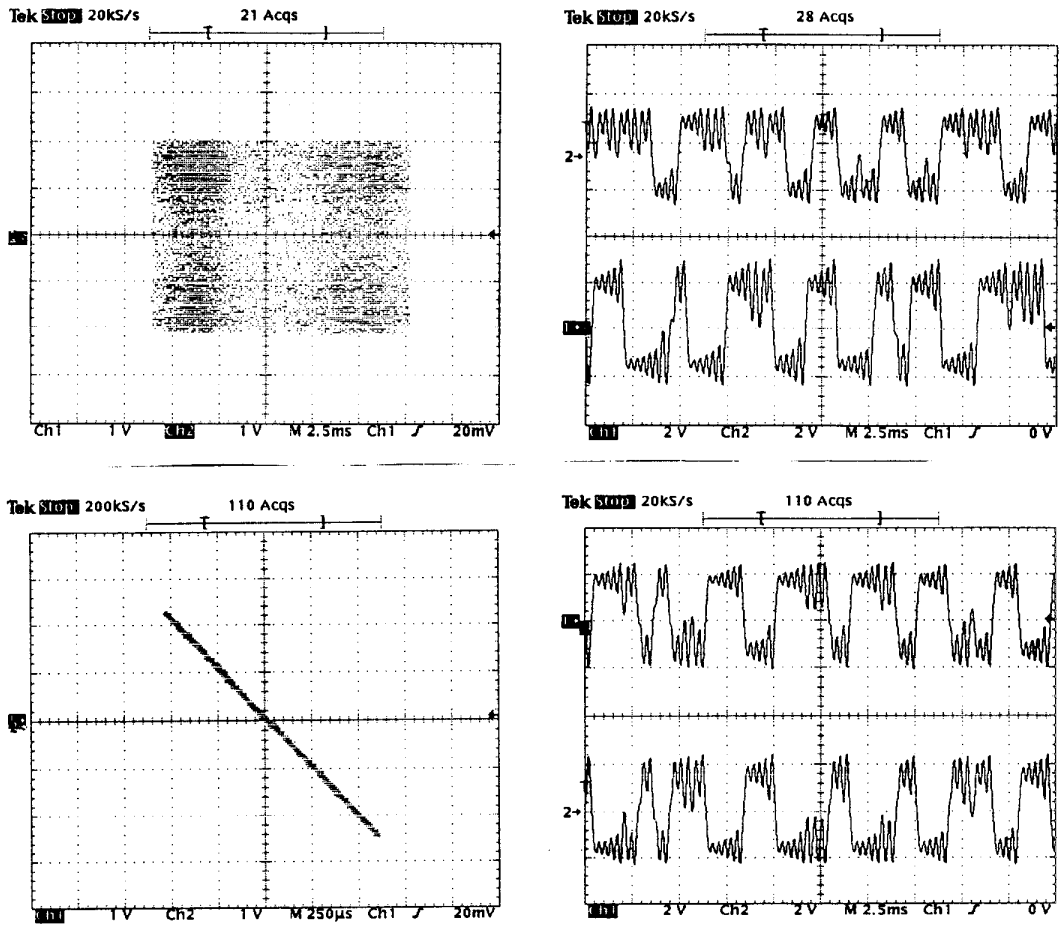


Figure 4: XY and time domain plots of the voltages across the Chua's diodes for the uncoupled (top) and negatively coupled (bottom) cases for $g = -1\text{mA/V}$.

Circuit Type	Numbers
Difference Amplifier [6]	6,9,14,17
Improved Howland Current Source [7]	1,5
Improved Precision Rectifier [6]	3,8,15,18
Inverting Amplifier [6]	4
Summer [6]	10,12,21
Unity Gain Buffer	2,7,11,13,16,19,20,22

Table 2: Circuits required for the voltage-based implementation

$1/(2R_C)$ the desired characteristic is obtained. The voltage V_2 is used to set the zero-crossing points of the three circuits via the reference voltages. This requires additional circuitry to connect either V_2 , $-V_2$, or ground to these reference voltages as in Table 1. V_1 acts as the excitatory input. This approach has not been fully investigated.

3. CONCLUSIONS

We have described a voltage and a current based circuit approach to the implementation of a piecewise linear circuit which enables synchronization and anti-synchronization of a pair of Chua's oscillators. Such a circuit may be used to realize the chaotic associative memory described in [4]. Initial experimental results confirm the overall design con-

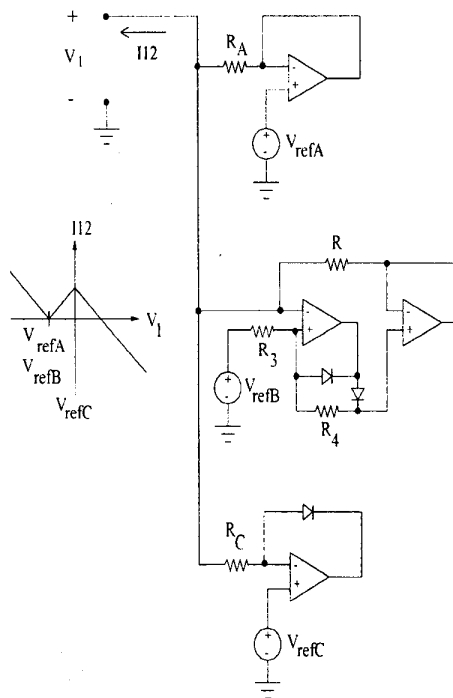


Figure 5: Schematic of the current-based circuit to generate I_{12} . The transfer characteristic is for $V_{REFA} = V_{REFB}$ and $V_{REFC} = 0$.

cepts. Further testing is required to verify complete circuit functionality.

The overall goal of our research is to produce an inexpensive and easily built circuit to enable construction of a reasonably sized chaotic associative memory with an eye towards an integrated circuit implementation. The circuit of Figure 3 requires far too many operational amplifiers to meet this need and thus this design may be regarded as a proof-of-concept rather than a practical implementation. The current-based approach should reduce the parts count considerably. Using analog switches to select desired circuit configurations might also lower the number of required components. We are currently designing a discrete component version of the coupling circuit.

4. ACKNOWLEDGMENTS

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