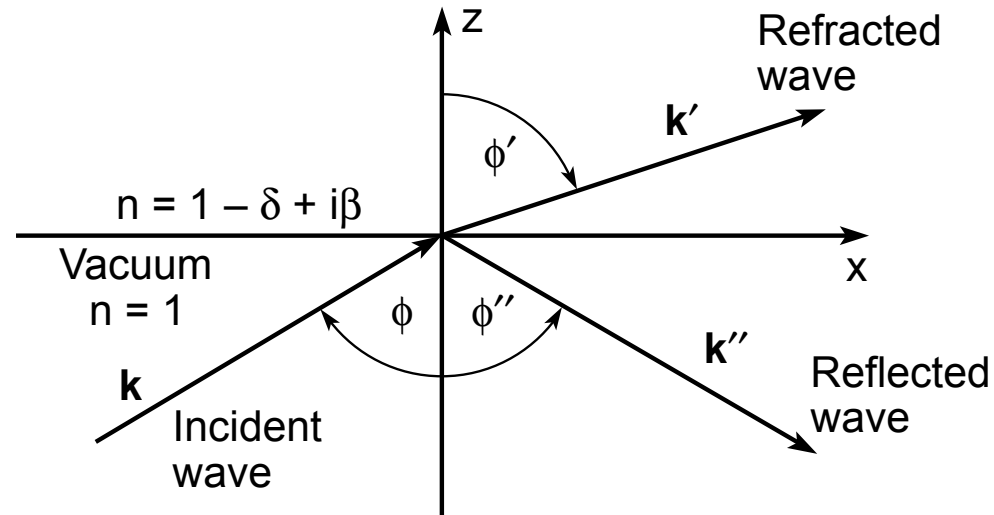




Reflection and Refraction at an Interface, Total Internal Reflection, Brewster's Angle



incident wave: $\mathbf{E} = \mathbf{E}_0 e^{-i(\omega t - \mathbf{k} \cdot \mathbf{r})}$ (3.30a)

refracted wave: $\mathbf{E}' = \mathbf{E}'_0 e^{-i(\omega t - \mathbf{k}' \cdot \mathbf{r})}$ (3.30b)

reflected wave: $\mathbf{E}'' = \mathbf{E}''_0 e^{-i(\omega t - \mathbf{k}'' \cdot \mathbf{r})}$ (3.30c)

- (1) All waves have the same frequency, ω , and $|\mathbf{k}| = |\mathbf{k}''| = \frac{\omega}{c}$
- (2) The refracted wave has phase velocity

$$V_\phi = \frac{\omega'}{k'} = \frac{c}{n}, \text{ thus } k' = |\mathbf{k}'| = \frac{\omega}{c} (1 - \delta + i\beta)$$



Boundary Conditions at an Interface

- **E** and **H** components parallel to the interface must be continuous

$$\mathbf{z}_0 \times (\mathbf{E}_0 + \mathbf{E}_0'') = \mathbf{z}_0 \times \mathbf{E}_0' \quad (3.32a)$$

$$\mathbf{z}_0 \times (\mathbf{H}_0 + \mathbf{H}_0'') = \mathbf{z}_0 \times \mathbf{H}_0' \quad (3.32b)$$

- **D** and **B** components perpendicular to the interface must be continuous

$$\mathbf{z}_0 \cdot (\mathbf{D}_0 + \mathbf{D}_0'') = \mathbf{z}_0 \cdot \mathbf{D}_0' \quad (3.32c)$$

$$\mathbf{z}_0 \cdot (\mathbf{B}_0 + \mathbf{B}_0'') = \mathbf{z}_0 \cdot \mathbf{B}_0' \quad (3.32d)$$



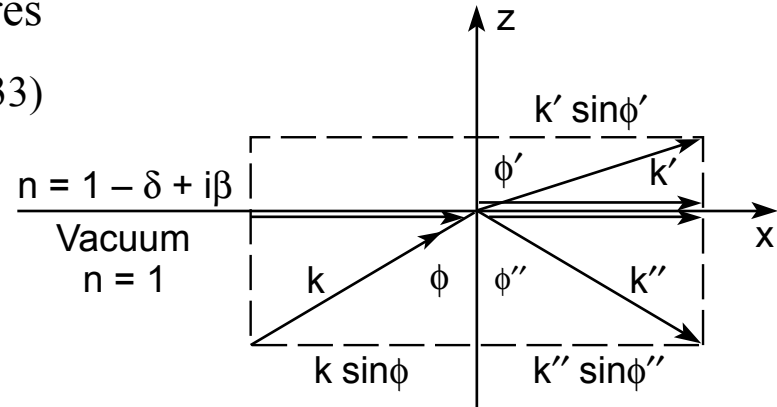
Spatial Continuity Along the Interface

Continuity of parallel field components requires

$$(\mathbf{k} \cdot \mathbf{x}_0 = \mathbf{k}' \cdot \mathbf{x}_0 = \mathbf{k}'' \cdot \mathbf{x}_0) \quad \text{at } z = 0 \quad (3.33)$$

$$k_x = k'_x = k''_x \quad (3.34a)$$

$$k \sin \phi = k' \sin \phi' = k'' \sin \phi'' \quad (3.34b)$$



Conclusions:

Since $k = k''$ (both in vacuum)

$$\sin \phi = \sin \phi'' \quad (3.35a)$$

$$\therefore \boxed{\phi = \phi''} \quad (3.35b)$$

The angle of incidence equals the angle of reflection

$$k \sin \phi = k' \sin \phi' \quad (3.36)$$

$$k = \frac{\omega}{c} \quad \text{and} \quad k' = \frac{\omega'}{c/n} = \frac{n\omega}{c}$$

$$\sin \phi = n \sin \phi'$$

$$\boxed{\sin \phi' = \frac{\sin \phi}{n}} \quad (3.38)$$

Snell's Law, which describes refractive turning, for complex n.



Total External Reflection of Soft X-Rays and EUV Radiation

Snell's law for a refractive index of $n \simeq 1 - \delta$, assuming that $\beta \rightarrow 0$

$$\sin \phi' = \frac{\sin \phi}{1 - \delta} \quad (3.39)$$

Consider the limit when $\phi' \rightarrow \frac{\pi}{2}$

$$1 = \frac{\sin \phi_c}{1 - \delta}$$

$$\sin \phi_c = 1 - \delta \quad (3.40)$$

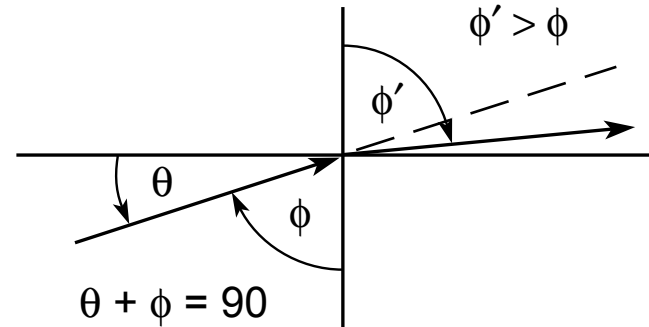
$$\sin(90^\circ - \theta_c) = 1 - \delta$$

$$\cos \theta_c = 1 - \delta$$

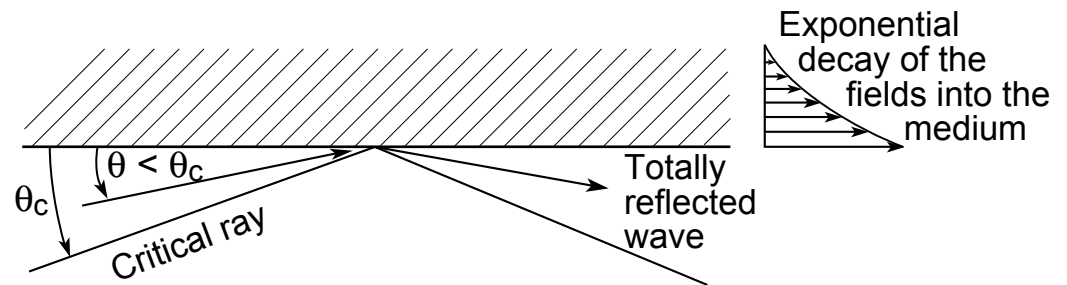
$$1 - \frac{\theta_c^2}{2} + \dots = 1 - \delta$$

$$\boxed{\theta_c = \sqrt{2\delta}} \quad (3.41)$$

The critical angle for total external reflection.



Glancing incidence ($\theta < \theta_c$) and total external reflection





Total External Reflection (continued)

$$\boxed{\theta_c = \sqrt{2\delta}} \quad (3.41)$$

$$\delta = \frac{n_a r_e \lambda^2 f_1^0(\lambda)}{2\pi}$$

$$\theta_c = \sqrt{2\delta} = \sqrt{\frac{n_a r_e \lambda^2 f_1^0(\lambda)}{\pi}} \quad (3.42a)$$

The atomic density n_a , varies slowly among the natural elements, thus to first order

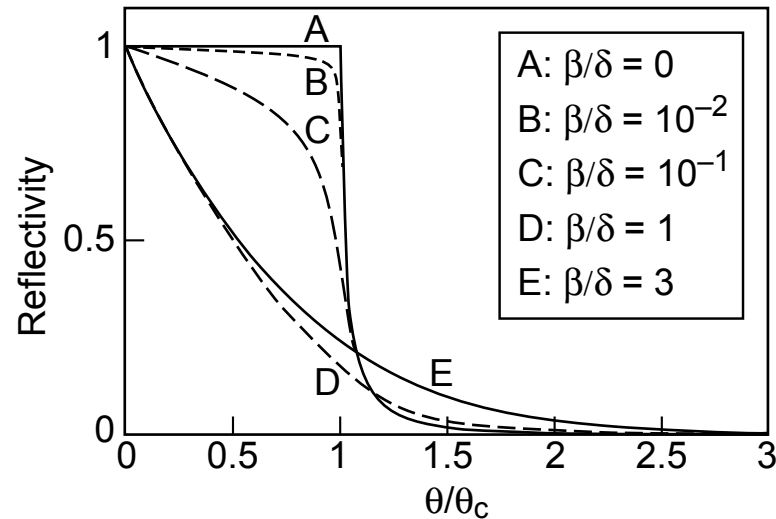
$$\theta_c \propto \lambda \sqrt{Z} \quad (3.42b)$$

where f_1^0 is approximated by Z . Note that f_1^0 is a complicated function of wavelength (photon energy) for each element.



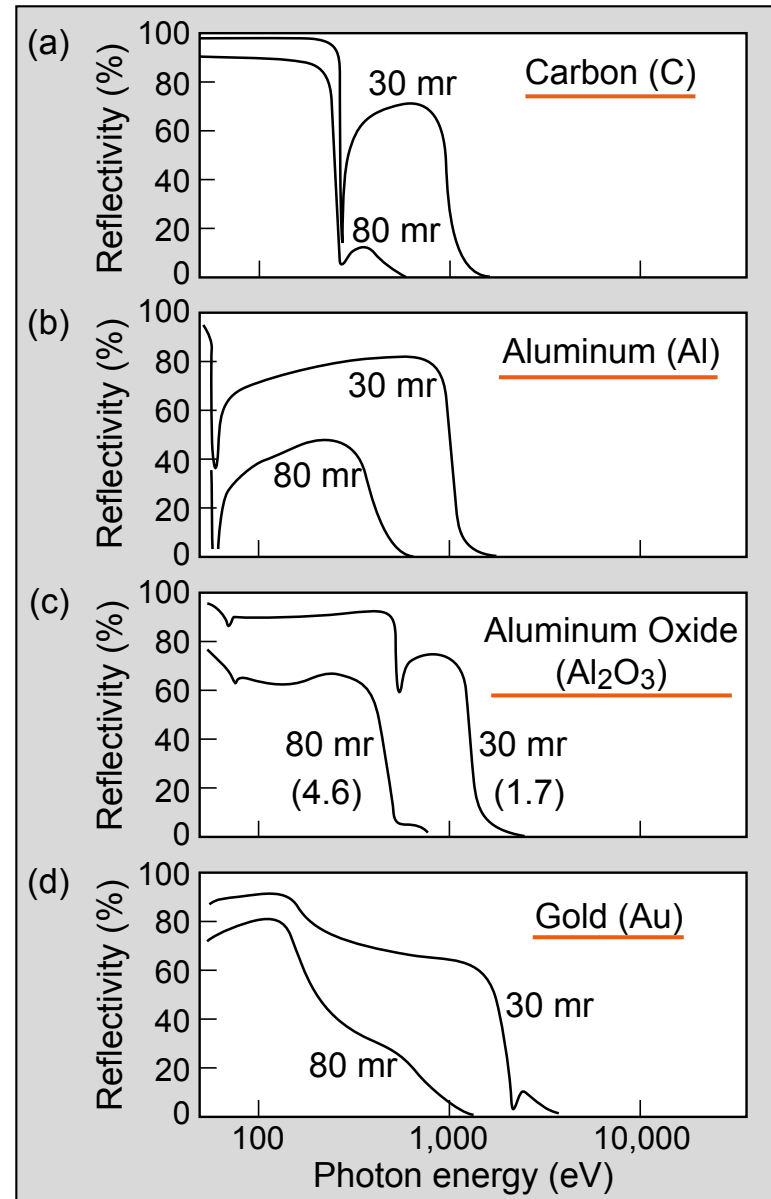
Total External Reflection with Finite b

Glancing incidence reflection
as a function of β/δ



- finite β/δ rounds the sharp angular dependence
- cutoff angle and absorption edges can enhance the sharpness
- note the effects of oxide layers and surface contamination

... for real materials

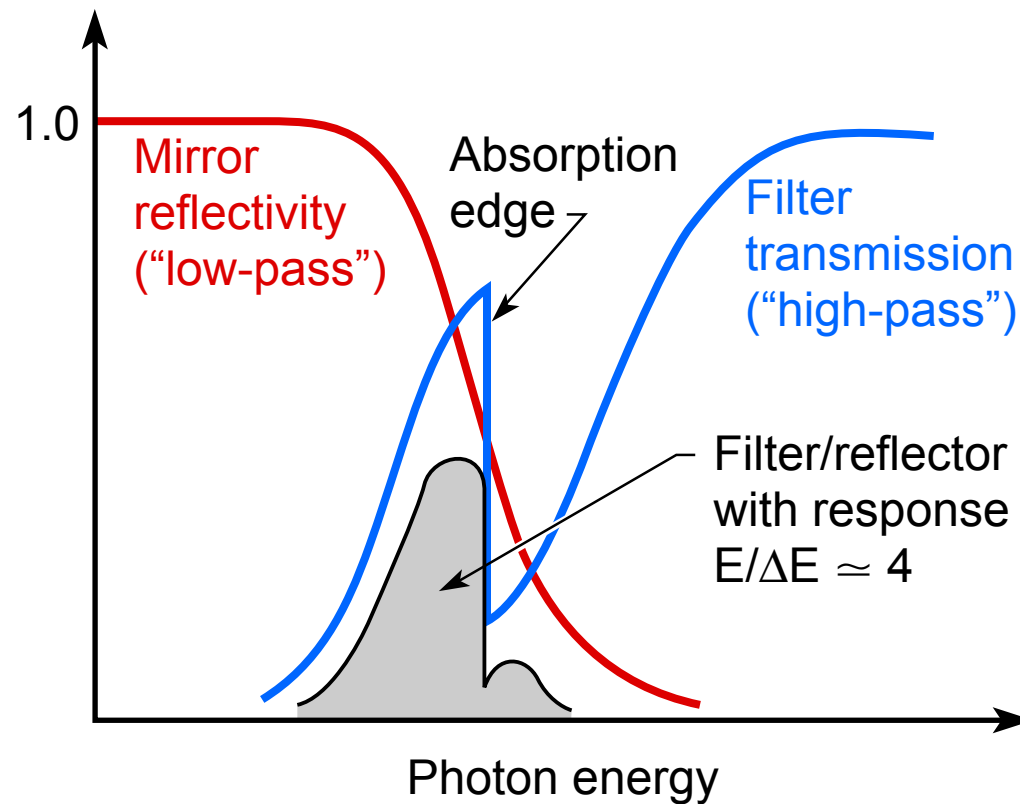


(Henke, Gullikson, Davis)



The Notch Filter

- Combines a glancing incidence mirror and a filter
- Modest resolution, $E/\Delta E \sim 3-5$
- Commonly used





Reflection at an Interface

E_0 perpendicular to the plane of incidence (s-polarization)

tangential electric fields continuous

$$E_0 + E_0'' = E_0' \quad (3.43)$$

tangential magnetic fields continuous

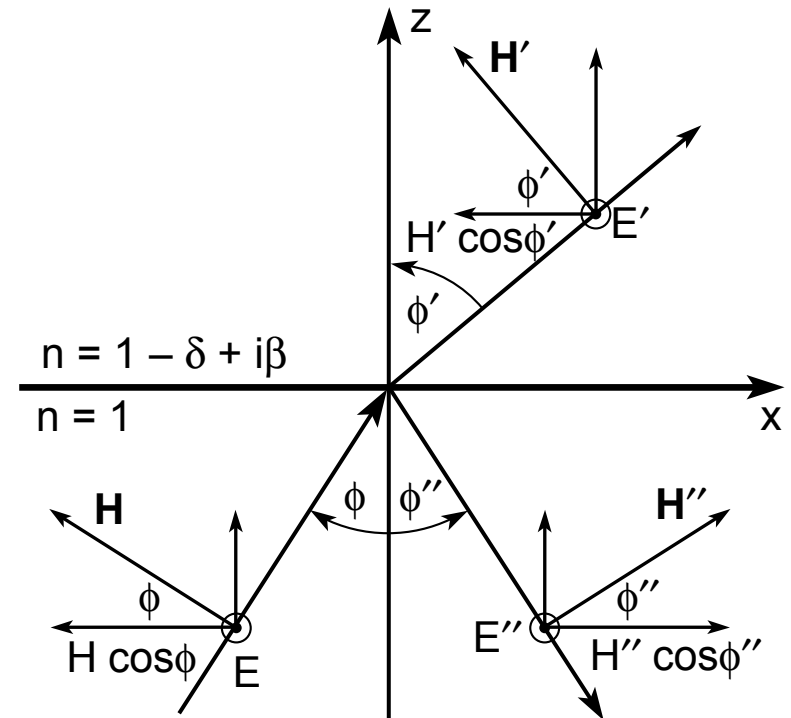
$$H_0 \cos \phi - H_0'' \cos \phi = H_0' \cos \phi' \quad (3.44)$$

$$\mathbf{H}(\mathbf{r}, t) = n \sqrt{\frac{\epsilon_0}{\mu_0}} \mathbf{k}_0 \times \mathbf{E}(\mathbf{r}, t) \Rightarrow H = n \sqrt{\frac{\epsilon_0}{\mu_0}} E$$

$$\sqrt{\frac{\epsilon_0}{\mu_0}} E_0 \cos \phi - \sqrt{\frac{\epsilon_0}{\mu_0}} E_0'' \cos \phi = n \sqrt{\frac{\epsilon_0}{\mu_0}} E_0' \cos \phi'$$

$$(E_0 - E_0'') \cos \phi = n E_0' \cos \phi' \quad (3.45)$$

Snell's Law: $\sin \phi' = \frac{\sin \phi}{n}$



Three equations in three unknowns (E_0' , E_0'' , ϕ') (for given E_0 and ϕ)



Reflection at an Interface (continued)

E_0 perpendicular to the plane of incidence (s-polarization)

$$\frac{E'_0}{E_0} = \frac{2 \cos \phi}{\cos \phi + \sqrt{n^2 - \sin^2 \phi}} \quad (3.47)$$

$$\frac{E''_0}{E_0} = \frac{\cos \phi - \sqrt{n^2 - \sin^2 \phi}}{\cos \phi + \sqrt{n^2 - \sin^2 \phi}} \quad (3.46)$$

The reflectivity R is then

$$R = \frac{\bar{I}''}{\bar{I}_0} = \frac{|\bar{\mathbf{S}}''|}{|\bar{\mathbf{S}}|} = \frac{\frac{1}{2} \text{Re}(\mathbf{E}''_0 \times \mathbf{H}_0^{''*})}{\frac{1}{2} \text{Re}(\mathbf{E}_0 \times \mathbf{H}_0^*)} \quad (3.48)$$

With $n = 1$ for both incident and reflected waves,

$$R = \frac{|E''_0|^2}{|E_0|^2}$$

Which with Eq. (3.46) becomes, for the case of perpendicular (s) polarization

$$R_s = \frac{\left| \cos \phi - \sqrt{n^2 - \sin^2 \phi} \right|^2}{\left| \cos \phi + \sqrt{n^2 - \sin^2 \phi} \right|^2} \quad (3.49)$$



Normal Incidence Reflection at an Interface

Normal incidence ($\phi = 0$)

$$R_s = \frac{|\cos \phi - \sqrt{n^2 - \sin^2 \phi}|^2}{|\cos \phi + \sqrt{n^2 - \sin^2 \phi}|^2} \quad (3.49)$$

$$R_{s,\perp} = \frac{|1 - n|^2}{|1 + n|^2} = \frac{(1 - n)(1 - n^*)}{(1 + n)(1 + n^*)}$$

For $n = 1 - \delta + i\beta$

$$R_{s,\perp} = \frac{(\delta - i\beta)(\delta + i\beta)}{(2 - \delta + i\beta)(2 - \delta - i\beta)} = \frac{\delta^2 + \beta^2}{(2 - \delta)^2 + \beta^2}$$

Which for $\delta \ll 1$ and $\beta \ll 1$ gives the reflectivity for x-ray and EUV radiation at normal incidence ($\phi = 0$) as

$$\boxed{R_{s,\perp} \simeq \frac{\delta^2 + \beta^2}{4}} \quad (3.50)$$

Example: Nickel @ 300 eV (4.13 nm)

From table C.1, p. 433	}	$R_{\perp} = 4.58 \times 10^{-5}$
$f_1^0 = 17.8$		
$f_2^0 = 7.70$		
$\delta = 0.0124$ $\beta = 0.00538$		



Glancing Incidence Reflection (s-polarization)

$$R_s = \frac{|\cos \phi - \sqrt{n^2 - \sin^2 \phi}|^2}{|\cos \phi + \sqrt{n^2 - \sin^2 \phi}|^2} \quad (3.49)$$

For $\theta = 90^\circ - \phi \leq \theta_c$

where $\theta_c = \sqrt{2\delta} \ll 1$

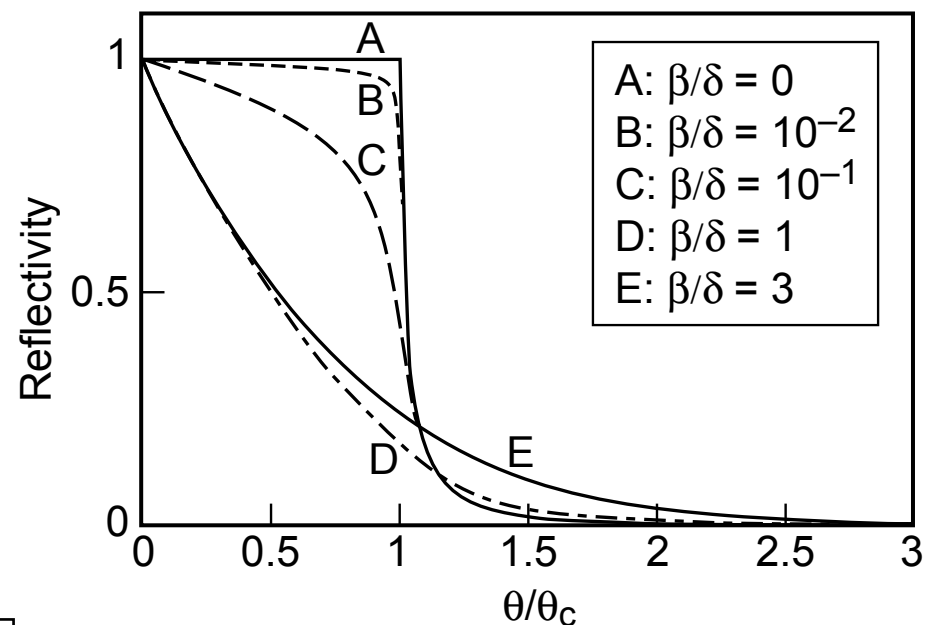
$$\cos \phi = \sin \theta \simeq \theta$$

$$\sin^2 \phi = 1 - \cos^2 \phi = 1 - \sin^2 \theta \simeq 1 - \theta^2$$

For $n = 1 - \delta + i\beta$

$$n^2 = (1 - \delta)^2 + 2i\beta(1 - \delta) - \beta^2$$

$$R_{s,\theta} = \frac{|\theta - \sqrt{(\theta^2 - \theta_c^2) + 2i\beta}|^2}{|\theta + \sqrt{(\theta^2 - \theta_c^2) + 2i\beta}|^2} \quad (\theta \ll 1)$$



E. Nähring, “Die Totalreflexion der Röntgenstrahlen”, Physik. Zeitstr. XXXI, 799 (Sept. 1930).



Reflection at an Interface

E_0 perpendicular to the plane of incidence (p-polarization)

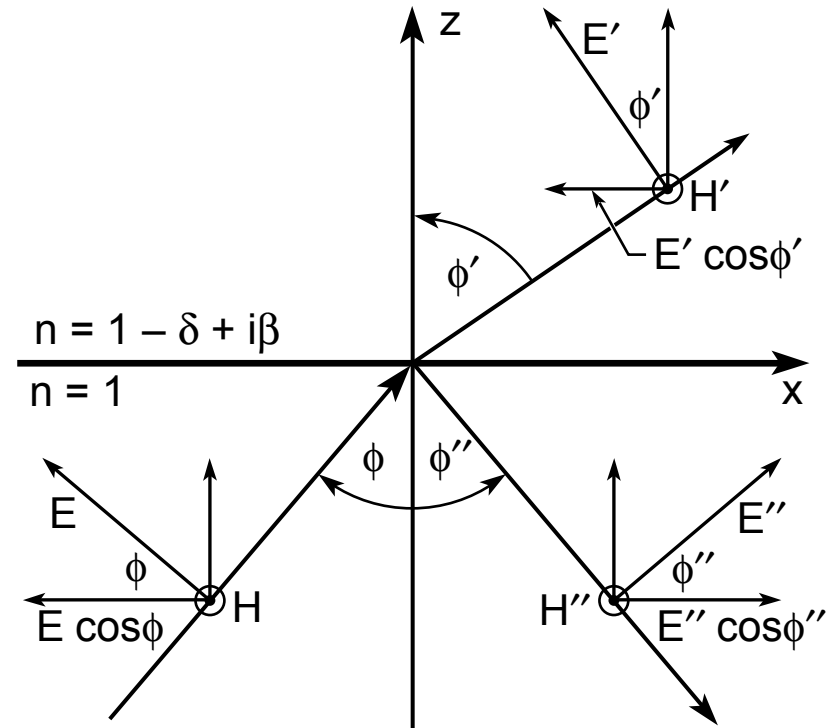
$$\frac{E_0''}{E_0} = \frac{n^2 \cos \phi - \sqrt{n^2 - \sin^2 \phi}}{n^2 \cos \phi + \sqrt{n^2 - \sin^2 \phi}} \quad (3.54)$$

$$\frac{E_0'}{E_0} = \frac{2n \cos \phi}{n^2 \cos \phi + \sqrt{n^2 - \sin^2 \phi}} \quad (3.55)$$

The reflectivity for parallel (p) polarization is

$$R_p = \left| \frac{E_0''}{E_0} \right|^2 = \frac{\left| n^2 \cos \phi - \sqrt{n^2 - \sin^2 \phi} \right|^2}{\left| n^2 \cos \phi + \sqrt{n^2 - \sin^2 \phi} \right|^2} \quad (3.56)$$

which is similar in form but slightly different from that for s-polarization. For $\phi = 0$ (normal incidence) the results are identical.





Brewster's Angle for X-Rays and EUV

For p-polarization

$$R_p = \left| \frac{E_0''}{E_0} \right|^2 = \frac{\left| n^2 \cos \phi - \sqrt{n^2 - \sin^2 \phi} \right|^2}{\left| n^2 \cos \phi + \sqrt{n^2 - \sin^2 \phi} \right|^2} \quad (3.56)$$

There is a minimum in the reflectivity where the numerator satisfies

$$n^2 \cos \phi_B = \sqrt{n^2 - \sin^2 \phi_B} \quad (3.58)$$

Squaring both sides, collecting like terms involving ϕ_B , and factoring, one has

$$n^2(n^2 - 1) = (n^4 - 1) \sin^2 \phi_B$$

or
$$\sin \phi_B = \frac{n}{\sqrt{n^2 + 1}}$$

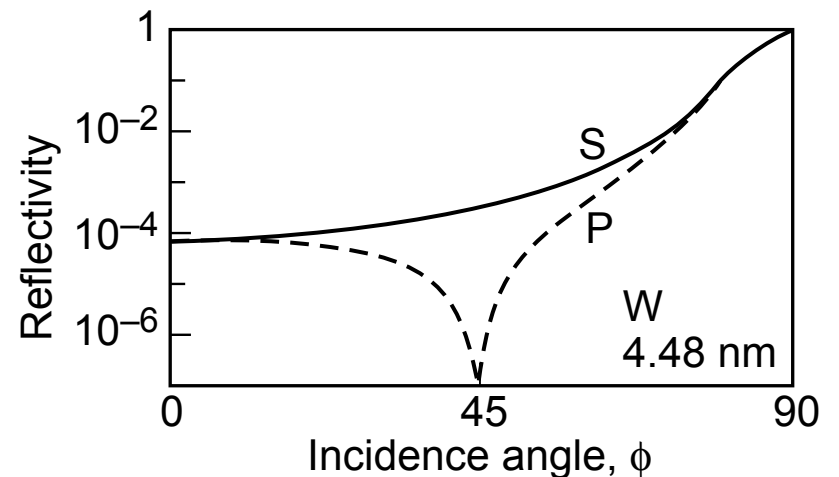
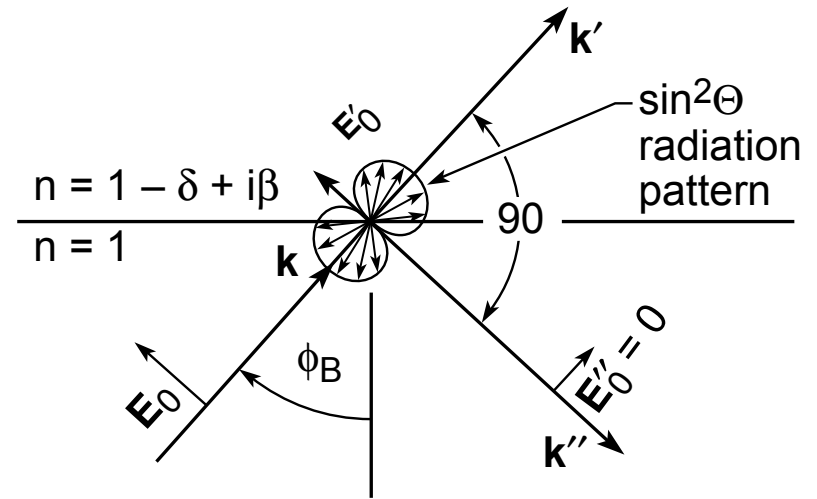
the condition for a minimum in the reflectivity, for parallel polarized radiation, occurs at an angle given by

$$\tan \phi_B = n \quad (3.59)$$

For complex n , Brewster's minimum occurs at

$$\tan \phi_B = 1 - \delta$$

or
$$\phi_B \simeq \frac{\pi}{4} - \frac{\delta}{2} \quad (3.60)$$

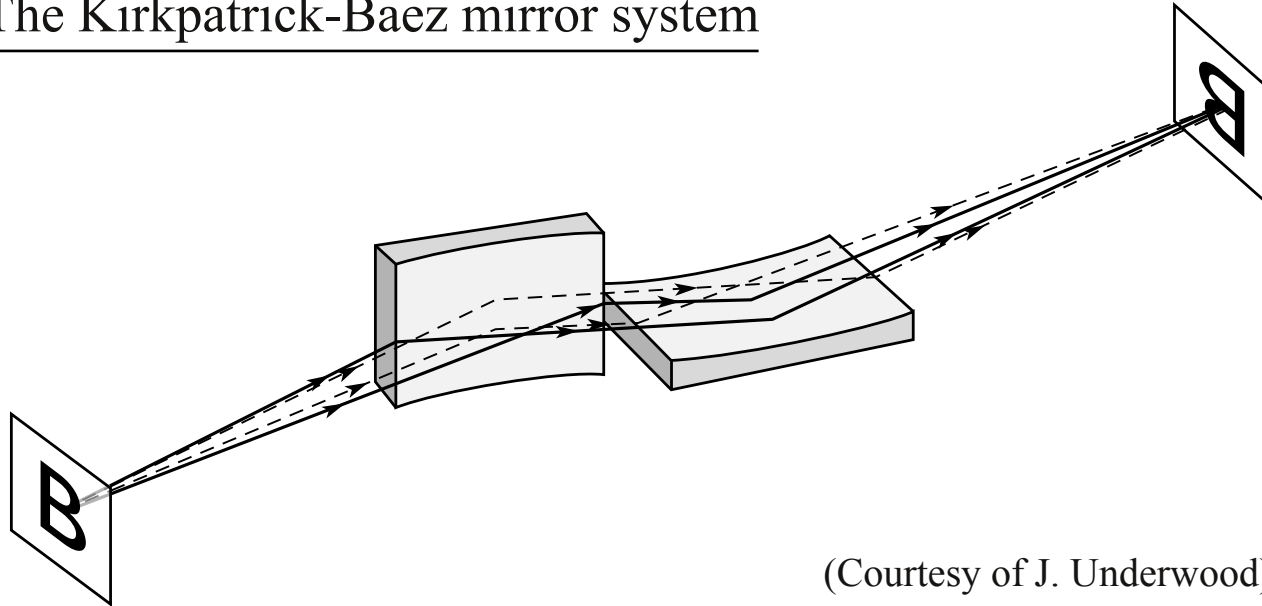


(Courtesy of J. Underwood)



Focusing with Curved, Glancing Incidence Optics

The Kirkpatrick-Baez mirror system



(Courtesy of J. Underwood)

- Two crossed cylinders (or spheres)
- Astigmatism cancels
- Fusion diagnostics
- Common use in synchrotron radiation beamlines
- See hard x-ray microprobe, chapter 4, figure 4.14



Determining f_1^0 and f_2^0

- f_2^0 easily measured by absorption
- f_1^0 difficult in SXR/EUV region
- Common to use Kramers-Kronig relations

$$f_1^0(\omega) = Z - \frac{2}{\pi} \mathcal{P}_C \int_0^\infty \frac{u f_2^0(u)}{u^2 - \omega^2} du \quad (3.85a)$$

$$f_2^0 = \frac{2\omega}{\pi} \mathcal{P}_C \int_0^\infty \frac{f_1^0(u) - Z}{u^2 - \omega^2} du \quad (3.85b)$$

as in the Henke & Gullikson tables (pp. 428-436)

- Possible to use reflection from clean surfaces; Soufli & Gullikson
- With diffractive beam splitter can use a phase-shifting interferometer; Chang et al.
- Bi-mirror technique of Joyeux, Polack and Phalippou (Orsay, France)